

Mathematical Models of Competitive Adsorption of Inorganic Anions in Soils

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Competition among anion species in solution for same sorption sites and soil surface can be of major significance in determining the effective mobility of any potentially adsorbing species. Major soil anion species include OH⁻, F⁻, Cl⁻, HCO₃⁻, CO₃⁻, NO₃⁻, SO₄²⁻, and PO₄³⁻. And some micro nutrients such as boron and molybdenum exist as H₂BO₃⁻ and MoO₄²⁻, as do some heavy metals such as chrome and arsenic as CrO₄²⁻ and HAsO₄²⁻. Pesticides such as 2,4,5-T and 2,4-D also exist as anions. Many anion species are retained by more complex mechanisms than the simple electrostatic attractions involved in most cation adsorption reactions. In binary system composed of two anions, the adsorption of one anion is influenced by the other anion due to the competition for the available and limited binding sites in soil constituents. The specifically adsorbed anions may compete more effectively for sorption sites than that of nonspecifically adsorbed anion. In this study, we aim to evaluate the mathematical models to determine the magnitude of concentration variations in adsorption due to competitive interactions between anions introduced to a system in binary mixtures.

Key words: Anion, Competitive Adsorption, Model, Soil

Summary of single-reaction models describing retention and release reactions in soil : reversible.

Order	Differential form	Integrated form
1st	$\frac{dC}{dt} = -k_1 \cdot C + k_2 \cdot S$	$\ln\left[1 + \frac{k_2}{k_1}\right] \left[\frac{C}{C_0} - \frac{k_2}{k_1}\right] = -(k_1 + k_2) \cdot t$
1st	$\frac{dC}{dt} = k'(C_s - C)$	$\ln\left[\frac{C_s - C}{C_s - C_0}\right] = -k' \cdot t$
2nd	$\frac{dC}{dt} = -k_1[C][\text{Site}] + k_2[C \cdot \text{Site}]$	$\ln\left[\frac{x_s(C_0 \cdot \text{Site}_0 - x \cdot x_s)}{(x_s - x)C_0^2 \cdot \text{Site}_0^2}\right] = \left[\frac{C_0^2 \cdot \text{Site}_0^2 - x_s^2}{x_s}\right] \cdot k_1 \cdot t$
nth	$\frac{dC}{dt} = -k_1 \cdot C^n + k_2 \cdot S$	$\left[\left(\frac{1}{C - C_s}\right)^{n-1}\right] = \left[\frac{1}{(C_0 - C_s)^{n-1}}\right] + (n-1) \cdot k \cdot t$

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Introduction

The mobility of anions in the aquatic environment is typically regulated by adsorption at the solid/water interface and by competition among various anion species for surface binding sites. The magnitude of these competitive interactions must be determined to predict and model anion migration (Wu et al., 2002). Competition between anions for sorption sites in soils occurs whenever a mixed fertilizer or pollutants are added to soil. Competition between anions involves not only physical competition for adsorption sites but also electrical effects which are the consequence of the changes in surface charge. However, the study of competitive adsorption of specifically adsorbed anions illustrates some of the difficulties which arise in interpretation of reactions at oxide/aqueous solution interfaces (Chung, 1993). At least two factors prevented a simple analysis of the reactions. First, at any pH value the maximum amount of adsorbate taken up at the surface depends on the identity of the anion, i.e., the adsorption envelopes are different for different anions. Second, it was necessary to postulate that the sites are of three kinds, common sites where both competitors can be adsorbed, sites where only one of the competitors can be adsorbed, and sites where only the other can be adsorbed.

Specific adsorption between competitive anions at aqueous solution/oxide interfaces involves formation of coordination complexes on the surface of oxide (Hingston et al., 1971). The oxide surface contains sites common to anions on which competitive adsorption takes place and sites on which only one or the other anion is able to adsorb. The number of sites at which competition takes place is almost equal to the number of sites available to the anions with the maximum adsorption in the presence of the competitors. However, there is a tendency for the number of sites for adsorption to decrease or increase with changing pH. Hingston et al. (1971) postulated that about 50 % of the total site occupied by adsorption from the mixtures of phosphate and arsenate do not exceed the sites which are occupied by the ion having the lowest adsorption in the absence of a competitor. The adsorption reactions are also mediated by the presence of protons, either on the oxide surfaces as a result of the normal charging process at pH values more acid than point of zero charge (Atkinson et al., 1971), or derived by dissociation of the conjugate acid of the anion (Hingston et al., 1971) when it is co-ordinated with the metal ion in the oxide surface.

There is considerable evidence of competition for the adsorption sites between organic ligands and inorganic anions, showing that adsorption of one species is reduced by the presence of a second species in binary systems (Hingston et al., 1971; Murali and Aylmore, 1983a,b Roy

and Griffin, 1986; Manning and Goldberg, 1997). Both organic and inorganic ions are capable of competing for sorption sites on soils. Potential competing chemical species include: phosphate, sulfate, selenite, molybdate, arsenate, bicarbonate, oxalate, citrate, and different phenols among the anions. Swenson et al. (1949) observed that certain organic acids were effective in reducing P sorption by iron and aluminum. It has become clear that there are many similarities among the adsorption reactions of different anions, and results obtained with one anion are an indication of what may happen with another anion. The present study was undertaken to understand that Mathematical models of competitive adsorption and their application can be used to determine the competitive adsorption of anions in binary solute mixtures for predicting the mobility of anions and a better understanding of the factors controlling anion availability in soils.

Mathematical models of competitive adsorption To fully comprehend adsorption mechanisms of anions in soil, a knowledge of the rate equations or rate law explaining the reaction system is required. A number of reactions have been employed to describe the kinetics of reactions in clay minerals and soils (Sparks and Jardine, 1981, 1987, 1989). These have included the first-order, second-order, Elovich, and zero-order reactions.

For a miscible displacement, the adsorption rate coefficient (K_a) defined for each flow rate in the system is constant if the rate of adsorption of an anion onto a colloidal surface follows first-order kinetics (Sparks et al., 1981). The forms of some equations for adsorption kinetics using a miscible displacement technique are given in Tables 1 and 2.

Under simple dynamic (time-dependent) adsorption models, the commonly used linear, Freundlich, and Langmuir-type isotherms are given by Eqs (1) to (4);

$$\frac{\partial S}{\partial t} = K_a \cdot C - K_d \cdot S \quad (\text{Eq. 1})$$

$$\frac{\partial S}{\partial t} = K_a \cdot C^n - K_d \cdot S \quad (\text{Eq. 2})$$

$$\frac{\partial S}{\partial t} = K_a \cdot C \cdot (Q - S) - K_d \cdot S \quad (\text{Eq. 3})$$

$$\frac{\partial S}{\partial t} = K_a \cdot C \cdot Q - K_d \cdot S \cdot (1 + K_m \cdot C) \quad (\text{Eq. 4})$$

where

Table 1. Summary of single-reaction models describing retention and release reactions in soil : reversible.

Order	Differential form	Integrated form
1st	$\frac{dC}{dt} = -k_1 \cdot C + k_2 \cdot S$	$\ln\left[1 + \frac{k_2}{k_1}\right] \left[\frac{C}{C_0} - \frac{k_2}{k_1}\right] = -(k_1 + k_2) \cdot t$
1st	$\frac{dC}{dt} = k'(C_s - C)$	$\ln\left(\frac{C_s - C}{C_s - C_0}\right) = -k' \cdot t$
2nd	$\frac{dC}{dt} = -k_1[C][\text{Site}] + k_2[\text{C-Site}]$	$\ln\left[\frac{x_s(C_0 \cdot \text{Site}_0 - x \cdot x_s)}{(x_s - x)C_0 \cdot \text{Site}_0}\right] = \left[\frac{C_0^2 \cdot \text{Site}_0^2 - x_s^2}{x_s}\right] \cdot k_1 \cdot t$
nth	$\frac{dC}{dt} = -k^1 \cdot C^n + k_2 \cdot S$	$\left[\left(\frac{1}{C - C_s}\right)^{n-1}\right] = \left[\frac{1}{(C_0 - C_s)^{n-1}}\right] + (n-1) \cdot k \cdot t$

S = concentration of metal retained by soil, mg kg⁻¹ or mol kg⁻¹.

Site = total concentration of reaction sites on soil, mg kg⁻¹ or mol kg⁻¹.

C-Site = concentration of metal-site complexes, mg kg⁻¹ or mol kg⁻¹.

C = concentration of metal in solution mg, L⁻¹ or mol L⁻¹.

C₀ and Site₀ = initial concentrations of reactants.

C_s = steady state concentrations of metal in solution.

x = C₀ - C.

x_s = C₀ - C_s.

k, k', k₁, k₂ are rate coefficients for kinetic models.

k' is the rate coefficient for the approach to steady state in the reversible 1st- and nth-order kinetics models.

n = reaction order.

a and b in the integrated irreversible 2nd-order kinetic model are stoichiometric coefficients.

Table 2. Summary of single-reaction models describing retention and release reactions in soils: irreversible.

Order	Differential form	Integrated form
1st	$\frac{dC}{dt} = -k \cdot C$	$\ln C = \ln C_0 - k \cdot t$
2nd	$\frac{dC}{dt} = -k \cdot [C][\text{Site}]$	$\ln(C/\text{Site}) = \ln\left(\frac{Cb}{\text{Site}_0}\right) + \frac{[(b \cdot C_0 - a \cdot \text{Site}_0) \cdot k \cdot t]}{a}$
nth	$\frac{dC}{dt} = -k \cdot C^n$	$\left(\frac{1}{C^{n-1}}\right) = \left(\frac{1}{C_0^{n-1}}\right) + (n-1) \cdot k \cdot t$

S = Concentration of metal retained by soil, mg kg⁻¹ or mol kg⁻¹.

Site = total concentration of reaction sites on soil, mg kg⁻¹ or mol kg⁻¹.

C-Site = concentration of metal-site complexes, mg kg⁻¹ or mol kg⁻¹.

C = concentration of metal in solution mg, L⁻¹ or mol L⁻¹.

C₀ and Site₀ = initial concentrations of reactants.

C_s = steady state concentrations of metal in solution.

x = C₀ - C.

x_s = C₀ - C_s.

k, k', k₁, k₂ are rate coefficients for kinetic models.

k' is the rate coefficient for the approach to steady state in the reversible 1st- and n_{th}-order kinetics models.

n = reaction order.

a and b in the integrated irreversible 2nd-order kinetic model are stoichiometric coefficients.

K_a and K_d = adsorption and desorption rate constant

K_m = equilibrium distribution coefficient (= K_a/K_d)

S = amount of anion adsorbed

C = concentration of anion in solution phase

n = Freundlich component

Q = maximum content sorbed.

However, it is difficult to describe competition between anions using these simpler models that have been shown to describe many aspects of the behavior of ions added singly to soil. It is because competition involves more than simple competition between anions for adsorption sites; it also involves the electrostatic consequences of the reaction between a surface and an ion. Reaction with an anion

makes the surface more negative (Barrow, 1989) and, therefore, less favorable for reaction with another anion. This effect has not been included in simpler models.

In most of the relevant literature, multicomponent adsorption has been quantified through Langmuir-type isotherms (Harter and Baker, 1977; Wu, 2000, 2002; Manning and Goldberg, 1996; Murali and Aylmore, 1983; Violante, 1991). Murali and Aylmore (1983a,b) described Langmuir- and Freundlich-type multicomponent isotherm equations, some of which have been applied to describe the adsorption of trace-level organic solutes by activated carbon.

An application of Langmuir-type isotherms (Murali and Aylmore, 1983a,b; Cho, 1985) to estimate the adsorption of multicomponent adsorption, particularly for a binary system, is given by reactions (Eq. 5) and (Eq. 6).

$$S_i = \frac{K_i C_i Q}{1 + \sum_j K_j C_j} \tag{Eq. 5}$$

where, i and j refer to the ith and jth species, respectively

Case 1. Extremely low effective concentrations ($S_i, S_j \ll Q$)

$$S_i = K_i \cdot C_i \cdot Q \tag{Eq. 6}$$

This suggests that at a low surface charge, the effects of competition are insignificant.

$$(S_j K_j C_j \gg 1 \text{ or } S_1 + S_2 = Q). \tag{Eq. 7}$$

Case 2. Binary system, high concentration. Under the conditions of near total surface charge,

$$S_1 = \frac{K_1 \cdot C_1 \cdot Q}{1 + K_1 \cdot C_1} \text{ and } S_2 = \frac{K_2 \cdot C_2 \cdot Q}{1 + K_1 \cdot C_1} \tag{Eq. 8}$$

Case 3. Binary system, one species stronger than the other, we obtain :

$$1 + K_1 \cdot C_1 + K_2 \cdot C_2 = 1 + K_1 \cdot C_1 \tag{Eq. 9}$$

Thus

$$S_1 = \frac{K_1 \cdot C_1 \cdot Q}{1 + K_1 \cdot C_1} \text{ and } S_2 = \frac{K_2 \cdot C_2 \cdot Q}{1 + K_1 \cdot C_1} \tag{Eq. 10}$$

The dynamic form of Langmuir-type adsorption equations in representing multiple-species adsorption in soil can be generalized as

$$\frac{\partial S_i}{\partial t} = K_{ai} \cdot C_i \cdot [Q - \sum_j S_j] - K_{di} \cdot S_i \tag{Eq. 11}$$

Note that contrary to the equation of Sheindorf et al. (year), Fritz-Schundler equations predict the possibility of the competition even when single-species isotherms are linear.

Roy et al. (1986) applied a multicomponent Freundlich-type equation, the Sheindorf- Rebhun-Sheintuch (SRS) equation (Sheindorf et al., 1981), to the adsorption of binary-solute mixtures containing arsenate-phosphate, and arsenate-molybdate. The associated competitive coefficient for each solute-soil system was viewed as a measurement of the relative affinity each soil has for a particular anion from an anionic mixture. Their expression of a competitive adsorption coefficient can be written for the adsorption of solute 1 from a binary mixture as

$$(x/m)_i^j = K_{fi} \cdot C_i \cdot (\sum_j A_{ij} \cdot C_j)^{1/(n_i)-1} \tag{Eq. 12}$$

where

$(x/m)_i^j$ = the amount of solute 1 adsorbed in the presence of solute 2,

C_1 and C_2 = the equilibrium concentrations of solutes 1 and 2,

K_{fi} and n = the Freundlich constants, vis

$$S = K_f C^{1/n}$$

and the a_{ij} term is defined as a competitive coefficient by Sheindorf et al. (1981).

where

$$a_{ij} = (B_j/C_j) \cdot C_i/C_j \tag{Eq. 13}$$

$$a_{ji} = (B_j/C_i) \cdot C_j/C_i \tag{Eq. 14}$$

$$B_i = (K_{fi} \cdot C_i/S_i)^{n_i/(n_i-1)} \tag{Eq. 15}$$

Discussion

The adsorption isotherms derived from ion exchange expressions corresponding to different exchange pairs were used to construct the source and sink terms of the transport equations. The models reviewed may seem complex, there are, in fact, simplifications of reality. To predict the movement of anions in soils, the effects of competitive adsorption among anions are seldom accounted for in the simpler mathematical models used. Therefore, a more complex model would be required if the reaction were to be followed by competing anions for sorption sites through time. This is because many anions that react with soil

continue to react for a very long period. Therefore, we need to develop the mathematical model for the description of multi-solute-adsorption based on the nature of the competing species in a given soil conditions including such factors as pH, solution concentration, and so on. Particularly, the associated competitive coefficient for each solute-soil system should be viewed as a measurement of the relative affinity each soil has for a particular anion from an anionic mixture.

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