

A Study on Reducing Vibration of Washing Machine Using Gyroscope System

* . † . *

Gyusung Na, Youngjin Park and Youn-sik Park

(Received November 21, 2013 ; Revised November 21, 2013 ; Accepted December 31, 2013)

Key Words : Gyroscope System(), Transient Vibration(), Active Vibration Control (), Multibody Dynamics()

ABSTRACT

A novel method to reduce the vibration of drum type washing machine is proposed. Recently, as the capacity of the drum-type washing machine gets expanded and its washing performance is improved, its market share is increasing in the whole world. But, the capacity of washing machine is limited because of door size and built-in washing machine size. The vibration of washing machine is caused by unbalanced cloths in high spinning drum, and the displacement of tub is maximized at transient range about 3 Hz(180 rpm). Previous researches were concerned about steady-state vibration in spinning. In this study, concerned about transient vibration and the displacement of tub is decreased by using gyroscope system. Mutibody dynamic model of washing machine include gyroscope is designed and the vibration of tub have been reduced by 44.7 % over original.

Nomenclature

I	inertia(kg·m ²)	가
θ	(°)	(top loading) (front loading)
ψ	Rotor (°)	.
$\dot{\psi}$	Rotor (rad/s)	(agitator)
ϕ	Gimbal (°)	(pulsator)
$\dot{\phi}$	Gimbal (rad/s)	(agitator) (pulsator)

† Corresponding Author ; Member, Department of Mechanical Engineering
 E-mail : yjpark@kaist.ac.kr
 Tel : +82-42-350-3060, Fax : +82-42-350-8220
 * KAIST, Department of Mechanical Engineering

A part of this paper was presented and selected as one of best papers at the KSNVE 2013 Annual Spring Conference
 ‡ Recommended by Editor SungSoo Na
 © The Korean Society for Noise and Vibration Engineering

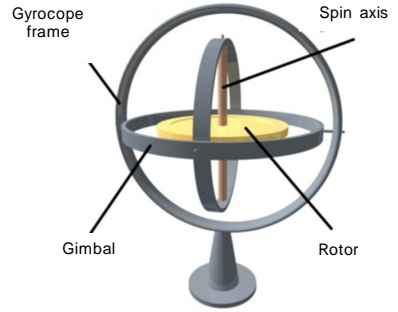


Fig. 1 Gyroscope model

(lifter)가
가 (weight balancer)
가 가
가

(mass) (inertia) (rotor)
(gimbal), (gimbal)
(gyroscope frame)

가 가 가
가 (rotor)
(tub) (drum) (frame) axis

Fig. 1

3

2

가

가
(1) (2) (3)
(active vibration control)
가 (free gyroscope)
(application)

가 (control moment gyroscope, CMG), (reaction wheel)
(momentum wheel),

가 가 가 가 (singularity)가

가 가 MEMS (4)
(CMG)

2.

(flywheel), (spin motor),
(gimbal motor)

2.1

(Gyroscope system)

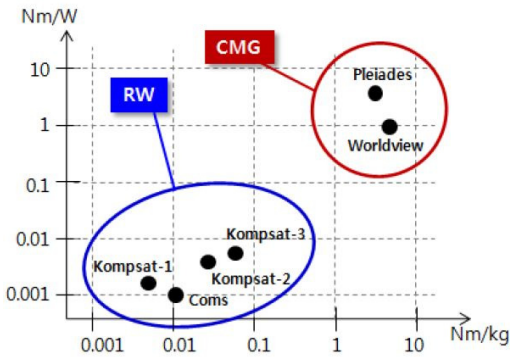


Fig. 2 Torque vs mass and power consumption⁽⁴⁾

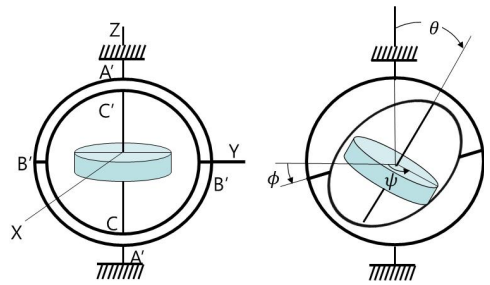


Fig. 3 Gyroscope model

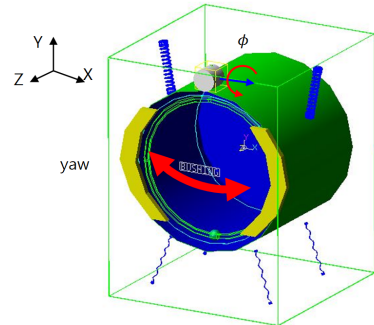


Fig. 4 Dynamic model of washing machine

가

가

Fig. 2 (RW)

(CMG)

가

2.2

Fig. 3 (rotor) C'-C (gimbal) B'-B (gyroscope frame) A'-A X, Y, Z θ, ϕ, ψ (3).

$$\omega = -\dot{\phi} \sin \theta i + \dot{\theta} j + (\dot{\psi} + \dot{\phi} \cos \theta) k \quad (1)$$

$$\theta, \dot{\phi}, \dot{\psi} \text{ (constant) (moment) } \quad (2)$$

$$\sum M_o = \{-I' \dot{\phi} \cos \theta + I(\dot{\psi} + \dot{\phi} \cos \theta)\} \dot{\phi} \sin \theta j \quad (2)$$

$$\theta = 90^\circ \quad (3)$$

$$\sum M_o = I \dot{\psi} \dot{\phi} j \quad (3)$$

(torque) (tub) (yaw motion) (3) I (ψ), $\dot{\psi}$ ($\dot{\phi}$) (gimbal)

2.3

(motor), (shaft), (frame), (weight balancer) 2 (spring), 4 (damper)

RecurDyn Fig. 4

(front) 500 g , 가 가

Fig. 5

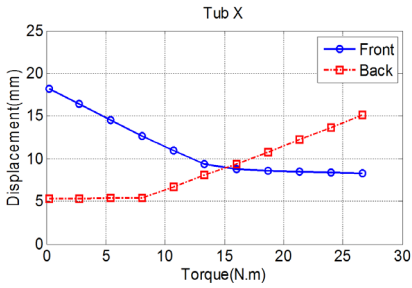


Fig. 5 Tub X vibration vs gyroscope torque

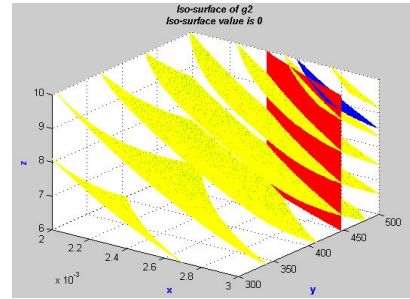


Fig. 6 Graphical solution

(tub) X . 12.8 N·m
 17.5 N·m (tub)
 10 mm .
 10 mm
 가 .

3.

3.1

$$x_1 = I, x_2 = \dot{\psi}, x_3 = \phi$$

$$f(X)$$

(kinetic energy)

(6)

$$f(X) : K.E.$$

$$g_1(X) : x_1 x_2 x_3 - 12.8 \geq 0$$

(4)

$$x_1 \geq 0; x_2 \geq 0; 0 \leq x_3 \leq 9.86$$

(4)

$g_1(x)$

$$12.8 \text{ N}\cdot\text{m}$$

가 (side constraint)

$$300 \text{ J}$$

. Fig. 6

Matlab

$$x_1 = 0.002839 \text{ kg}\cdot\text{m}^2, x_2 = 459.08 \text{ rad/s},$$

$$x_3 = 9.9 \text{ rad/s}$$

(7)

3.2

Table 1

(kinetic energy) 9435 J 299 J 97 %

가

Fig. 7

Fig. 8

Table 1 Comparing of simulation results

	Origin	Initial design parameter ⁽⁵⁾	Optimal design parameter
Inertia (kg·mm ²)		1404	2839
Rotor speed (rad/s)		3665	459
Gimbal speed (rad/s)		2.5	9.8
Kinetic energy (J)		9435	299
Tub X (mm)	17.9	10.5	9.9

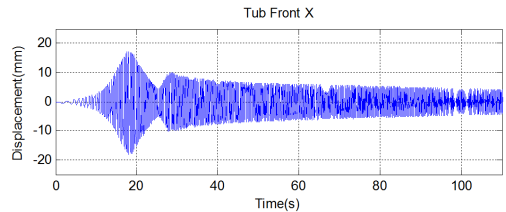


Fig. 7 Original tub vibration

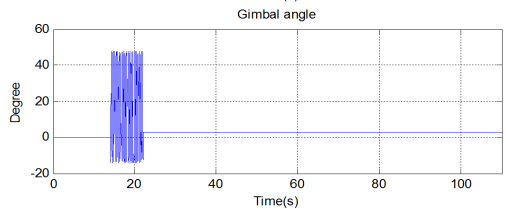
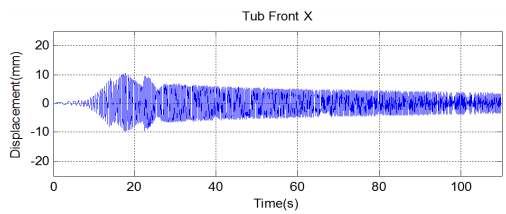


Fig. 8 Simulation results

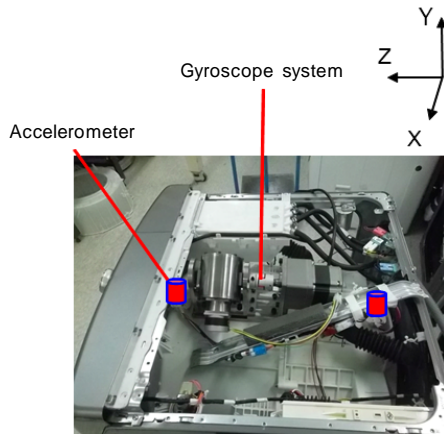


Fig. 9 Configuration of experimental setup

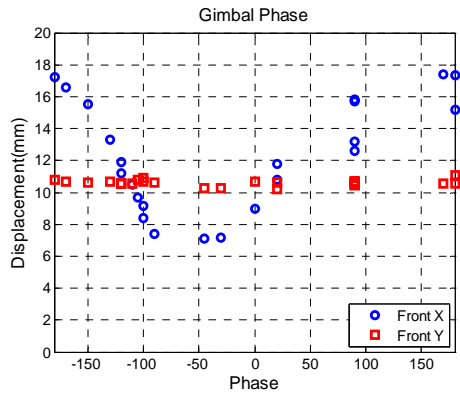


Fig. 10 Test results of front vibration

10 mm
Fig. 8
,
가

4.

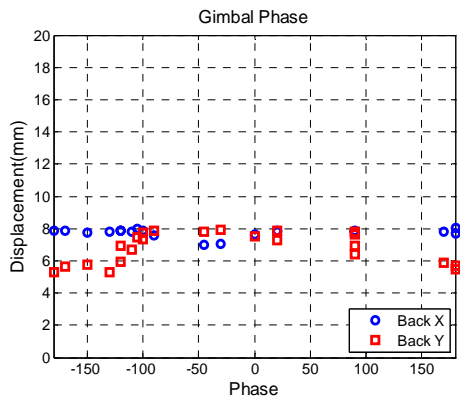


Fig. 11 Test results of back vibration

Fig. 9

(feasibility test)

, 가

(tub)

500 g

(open loop)

가

(gimbal)

X

180°

Fig. 10

(gimbal)

(phase delay)가 -90°

(Energy)

(water consumption)

가

가

가

-180°

가

가

가

-90°

가

Fig. 11

(X-axis)

(gap)가

, (inertia) = 2839 kg·mm², (rotor

) = 459 rad/s, (gimbal) =

9.9 rad/s

			97 %
	(kinetic energy)	.	
	(tub) X	17.9 mm	
9.9 mm	44.7 %	.	
	(feasibility test)	13.4 mm	
7.4 mm	44.7 %	가	

2013 ()

(No.2010-0028680).

References

(1) Lee, J., Jo, S., Kim, T. and Park, Y., 1998, Modeling and Dynamic Analysis of a Front Loaded Washing Machine with Ball Type Automatic Balancer, Transactions of the Korean Society for Noise and Vibration Engineering, Vol. 8, No. 4, pp. 670~682.

(2) Bae, S., Lee, J. M., Kang, Y. J. and Kang, J. S., 2002, Dynamic Analysis of an Automatic Washing Machine with a Hydraulic Balancer, Journal of Sound and Vibration, Vol. 257, No. 1, pp. 3~18.

(3) Moon, Y. J., 2005, Active Vibration Control System using Gyroscope for Structures, Ph.D. Thesis, Korea Advanced Institute of Science and Technology, Daejeon, Republic of Korea, pp. 12~15.

(4) Lee, S. H., 2012, Technology of Control Moment Gyroscope and its Industrial Trend, Proceedings of KSAS, Vol. 40, No. 1, pp. 86~92.

(5) Na, G. S., Park, Y. J., Park, Y. S. and Kang, J.

H., 2013, Washing Machine Vibration Analysis using Gyroscope System, Proceedings of the KSME Annual Spring Conference, pp. 35~36.

(6) Venkataraman, P., 2009, Applied Optimization with MATLAB Programming, John Wiley & Sons, New Jersey.

(7) Na, G. S., Park, Y. J. and Park, Y. S., 2013, Washing Machine Vibration Analysis using Gyroscope System, Proceedings of the KSNVE Annual fall Conference, pp. 35~36.



Gyusung Na, B.S. in SungKyun Kwan University, Mechanical Eng., 2002, M.S. in KAIST, 2012~Present, in Structural Dynamics and Applied Control Lab. Research interests are active vibration control, vibration analy-

sis and control.



Youngjin Park, B.S. in Seoul National University, Mechanical Eng., 1980, M.S. in Seoul National University, Mechanical Eng., 1982, Ph. D. in University of Michigan, 1987, University of Michigan Research Fellow, 1987~

1988, New Jersey Institute of Technology Assistant Professor, 1988~1990, KAIST Mechanical Eng. Professor, 1990~Present, in Structural Dynamics and Applied Control Lab. Research interests are automatic control, active and passive noise control, 3D sound technology, vehicle stability control, fault diagnosis, robust control and system identification.