# A Reliability Sampling Plan Based on Progressive Interval Censoring Under Pareto Distribution of Second Kind

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**Abstract.** In this paper, a reliability sampling plan under progressively type-1 interval censoring is proposed when the lifetime of products follows the Pareto distribution of second kind. We use the maximum likelihood estimator for the median life and its asymptotic distribution. The cost model is proposed and the design parameters are determined such that the given producer's and the consumer's risks are satisfied. Tables are given and the results are explained with examples.

**Keywords:** Acceptance Sampling, Cost Minimization, Pareto Distribution of Second kind, Maximum Likelihood Estimation

## 1. INTRODUCTION

The censoring schemes such as time censored (Type-I) and failure-censored (Type-II) are commonly used to reduce the time and the cost of the life test. In these censoring schemes the surviving items are only removed at the end of the life test. However, there is a situation in which experimenter needs to remove a part of the surviving items at time points before the termination time. This type of life test is called a progressive censoring. The basic advantage of progressive censoring scheme is that the removed items can be used for other

experiment. Secondly, this censoring scheme can be used to save the cost and the time of the experiment when the items under inspections are costly. For more details about the advantages of this scheme, reader may refer to Cohen (1963).

Many authors have studied on the inference of the parameters of various lifetime distributions under the progressively censoring. See for example, Ali Mousa and Jaheen (2002), Gouno *et al.* (2004), Guilbaud (2001), Li *et al.* (2007), Lin *et al.* (2006), Soliman (2005), Tse and Yuen (1998). Recently, Wu *et al.* (2008) proposed the progressively group-censoring life test considering

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the cost model for the Weibull distribution. Huang and Wu (2008) developed the reliability plans under the progressively Type-I interval censoring using the cost function. They determined the design parameter using the maximum likelihood estimation (MLE) method which minimizes the total cost of the experiment under the specified producer's and the consumer's risks. Wu and Huang (2009) developed the progressively Type-1 group censoring using the MLE to find the parameter of Weibull distribution. The design parameters using the cost model are determined and the sensitivity analysis is investigated. Recently, Lio et al. (2010a, b) proposed acceptance sampling plans for the Birnbaum-Saunders distributions and Burr type XII distributions using the median as the quality parameter. They showed and justified the use of median in area of reliability and argued that as distributions under study are skewed and for skewed distributions median provides better results than the mean as quality parameter. For more detail about these papers reader can refer to Lio et al. (2010a, b).

Exploring the literature about the progressively Type-1 censoring we see that most of the authors used the Weibull distribution to develop the plan based on this scheme. No attention has been paid to develop an acceptance sampling plan for the Pareto distribution of the second kind. So, the purpose of this paper is to design an acceptance sampling plan based on the progressive Type-I censoring scheme for the Pareto distribution of the second. The minimum sample size, the number of inspections and the length of the inspection interval will be determined to minimize the total cost while satisfying the given producer's and the consumer's risks. We use the median life of the Pareto distribution as a reliability measure.

#### 2. PROPOSED SAMPLING PLAN

An acceptance sampling plan is used to test the quality or reliability of the submitted lots of items before it is released for consumer's use. This quality is tested on the basis of a few items taken from a lot. We use the estimate of the median life as the test statistic

#### 2.1 Pareto Distribution of Second Kind

Suppose that an experimenter wants to conduct a life test under the assumption that the lifetime of products under inspection is independently and identically distributed as Pareto distribution of the second kind with the probability distribution function (pdf) and cumulative distribution function (cdf) given as

$$f(t) = \frac{\lambda t}{\sigma} \left( 1 + \frac{t}{\sigma} \right)^{-(\lambda + 1)} t > 0, \ \sigma, \ \lambda > 0$$
 (1)

and

$$F(t) = 1 - \left(1 + \frac{t}{\sigma}\right)^{-(\lambda)} t > 0, \quad \sigma, \quad \lambda > 0$$
 (2)

where  $\lambda$  is a shape parameter and  $\sigma$  is a scale parameter of the distribution. In this study we assume that  $\lambda$  is known. This distribution is frequently used in quality control and the reliability applications. Bain and Engelhardt (1992) discussed the application of this distribution in the field of bio-medical sciences. Baklizi (2003) proposed the ordinary single acceptance sampling plans based on truncated life test under the Pareto distribution of the second kind. More recently, Aslam *et al.* (2010) proposed the group acceptance sampling plans for the Pareto distribution of the second kind.

As stated in the above procedure we are using the median life of the distribution as a reliability measure. The median for the Pareto distribution is derived by

$$median = \sigma(2^{1/\lambda} - 1) \tag{3}$$

Particularly for  $\lambda=1$ , the median is just  $\sigma$ . When the shape parameter  $\lambda$  is known, the estimate of the median is just the constant times the estimate of  $\sigma$ . Therefore, we may assume that  $\lambda=1$  without loss of generality.

## 2.2 Procedure of the Proposed Plan

Let us consider the following sampling plan based on the life test with type-1 progressively interval censoring for the items whose life follows the Pareto distribution of the second kind given in Eq. (1) or Eq. (2). In this plan acceptance number c acts as the lower specification limit.

- Step 1: Draw a sample of size n and put them on test at time 0.
- Step 2: Items are inspected at pre-determined times  $\tau_1, \tau_2, \dots, \tau_n$ , where  $0 < \tau_1 < \tau_2 < \dots < \tau_n$ .
- $au_1, au_2, \cdots, au_k$ , where  $0 < au_1 < au_2 < \dots < au_k$ . Step 3: At the i-th inspection time the number of failed items  $(n_i)$  are counted, and  $r_i$  surviving items are removed for future use  $(i = 1, 2, \dots, k)$ .
- Step 4: Estimate the median of the distribution using the maximum likelihood estimation.
- Step 5: Accept the lot if the estimated median is greater than or equal to the acceptance number c. Reject the lot, otherwise.

Let  $m_i$  be the surviving items just before the i-th inspection time. Then, we have

$$m_i = m_{i-1} - n_{i-1} - r_{i-1}$$
,  $i = 2, \dots, k$ ;  $m_1 = n$ 

The value of  $r_i$ ,  $i = 1, 2, \dots k$  are assumed to be determined by pre-fixed proportion  $p_i(p_k = 1)$  of the remaining items as in Huang and Wu (2008) such

that

$$r_i = (m_i - n_i) p_i$$
, i=1, ..., k

Under a progressively type-1 censoring scheme, we have the fact that

$$n_i \mid n_{i-1}, \dots, n_1, r_{i-1}, \dots, r_1 \sim binomial(m_i, q_i)$$
 (4)

where  $q_i$  is the probability that an item fails between  $\tau_{i-1}$  and  $\tau_i$  and given by

$$q_{i} = \frac{\left(F(\tau_{i}) - F(\tau_{i-1})\right)}{1 - F(\tau_{i-1})} \tag{5}$$

For the distribution under study given (2), the Eq. (5) can be written as

$$q_{i} = \frac{\left(\sigma + \tau_{i}\right)^{\lambda} - \left(\sigma + \tau_{i-1}\right)^{\lambda}}{\left(\sigma + \tau_{i}\right)^{\lambda}} \tag{6}$$

Particularly for  $\lambda = 1$ , the above equation can be written as

$$q_{i} = \frac{\tau_{i} - \tau_{i-1}}{\sigma + \tau_{i}} \tag{7}$$

In fact, Step 5 in the above procedure represents the decision rule for the following hypothesis testing:

$$H_0: \sigma = \sigma_0 \text{ vs } H_1: \sigma = \sigma_1, \sigma_0 > \sigma_1$$
 (8)

where  $\sigma_0$  is the acceptable reliability level (ARL) and  $\sigma_1$  is lot tolerance reliability level (LTRL). As mentioned earlier, two types of risks are always associated with the acceptance sampling plans. The rejection of a good lot is called the producer's risk, say  $\alpha$  and the acceptance of a bad lot is called the consumer's risk, say  $\beta$ . We want to find the design parameter for the proposed plan such that the following two inequalities must satisfied

$$P\{\hat{\sigma} > c \mid \sigma = \sigma_0\} = 1 - \alpha \tag{9}$$

and

$$P\{\hat{\sigma} > c \mid \sigma = \sigma_1\} = \beta \tag{10}$$

where  $\hat{\sigma}$  is the estimator of  $\sigma$ .

### 2.3 Parameter Estimation

Given observations  $(n_1, n_2, \dots, n_k)$ , and  $(r_1, r_2, \dots, r_k)$ ,

the likelihood function is given as

$$lnL(\sigma) \propto \sum_{i=1}^{k} n_i \ln q_i + (m_i - n_i) \ln (1 - q_i)$$
 (11)

The maximum likelihood estimator (MLE) of  $\sigma$  can be obtained from the following equation:

$$\frac{\partial \ln L(\sigma)}{\partial \sigma} = \sum_{i=1}^{k} \frac{-n_i + m_i q_i}{(\sigma + \tau_i)(1 - q_i)} = 0$$
 (12)

Let  $\hat{\sigma}$  be the MLE of  $\sigma$ . Then, the asymptotic distribution of  $\hat{\sigma}$  is given as

$$\hat{\sigma} \sim Nor\left(\sigma, \frac{1}{I(\sigma)}\right)$$
 (13)

where  $I(\sigma)$  is the Fisher information which is given as

$$I(\sigma) = -E \left[ \frac{\partial^2 \ln L(\sigma)}{\partial \sigma^2} \right] = -E \left[ \sum_{i=1}^k \frac{n_i - 2m_i q_i + m_i q_i^2}{(1 - q_i)^2 (\sigma + \tau_i)^2} \right]$$
(14)

Since  $E[n_i] = q_i E[m_i]$  and

$$E(m_i) = \frac{n\sigma}{\sigma + \tau_{i-1}} \prod_{j=1}^{i-1} (1 - p_j)$$

 $I(\sigma)$  in (14) reduces to

$$I(\sigma) = -E\left(\frac{\partial^{2} \ln(\sigma)}{\partial \sigma^{2}}\right) = n\sigma \sum_{i=1}^{k} \frac{\prod_{j=1}^{i-1} (1-p_{j})}{(\sigma+\tau_{i})^{2}} \frac{\tau_{i} - \tau_{i-1}}{(\sigma+\tau_{i})^{2}}$$
(15)

If we suppose that the inspection interval have the same length and that the percentage of removal from each interval are the same such that  $\tau_i = i\tau$  and  $p_i = p$ , then the Eq. (15) can be written as

$$I(\sigma) = n\tau\sigma\sum_{i=1}^{k} \frac{(1-p)^{i-1}}{(\sigma+i\tau)^{2}} \frac{1}{(\sigma+(i-1)\tau)^{2}}$$
(16)

## 3. DESIGN OF SAMPLING PLAN USING COST FUNCTION

Let us define

$$V = 1/I(\sigma) \tag{17}$$

According to Huang and Wu (2008), the sample size n and the acceptance number c of the proposed sampling plan satisfying the producer's risk  $\alpha$  and the consumer's risk β are given by

$$n = \left(\frac{z_{\beta}\sqrt{V_1} - z_{1-\alpha}\sqrt{V_0}}{\sigma_0 - \sigma_1}\right)^2, \tag{18}$$

and

$$c = \frac{z_{1-\alpha}\sqrt{V_0}\sigma_1 - z_{\beta}\sqrt{V_1}\sigma_0}{z_{1-\alpha}\sqrt{V_0} - z_{\beta}\sqrt{V_1}},$$
(19)

where  $z_{\gamma}$  is the  $\gamma$  percentile of a standard normal distribution,  $V_0$  is the value of V at ARL and  $V_1$ is the value of V at LTRL.

In this paper, we consider the same cost function as proposed by Huang and Wu (2008) in order to determine the sample size and the acceptance number. Let C be the cost of installing all test items in the beginning of a life test (setup cost) and  $C_s$  be the cost of testing each item. Also let  $C_i$  be the cost of one inspection and  $C_0$  be the operation cost per unit time. Then, the total cost required for the proposed sampling plan based on the progressive censoring scheme will be

$$TC(n, k, \tau) = C_a + nC_s + kC_i + k\tau C_0$$
 (20)

To obtain the design parameters  $(n, c, k, \tau)$  of the proposed sampling plan we solve the following optimization problem:

Minimize  $TC(n, k, \tau) = C_a + nC_c + kC_i + k\tau C_0$  (21a)

Subject to 
$$n = \left(\frac{z_{\beta}\sqrt{V_1} - z_{1-\alpha}\sqrt{V_0}}{\sigma_0 - \sigma_1}\right)^2, \quad (21b)$$

Note that the acceptance number c is not involved in the above optimization problem. So the parameters n,k and  $\tau$  will be obtained from the above problem and c will be derived from Eq. (19).

We find the design parameters as well as the total cost required for given values of p and  $\sigma_0$  in Table 1~Table 4. Here we assume that  $\sigma_1 = \xi \sigma_0$ . As in Huang and Wu (2008), it is assumed that  $C_a = 10C_s$ ,  $C_i = 0.5C_s$  and  $C_o = 0.1C_s$  and that  $C_s = 1$ .

From these tables, it is clear that as the value of  $\xi$  is increased for the same values of p and  $\sigma_0$ , the design parameters such as n, k and total cost are increased. Larger value of  $\xi$  indicates more strict reli

**Table 1.** Optimal acceptance number c and disposition of life test  $(n, k, \tau)$  for  $\alpha = 0.05$  and  $\beta = 0.05$ 

	ics	si (n	$(\kappa, \kappa, \iota)$ 10	1 α	= 0.03	and $\beta =$	0.03.
p	$\sigma_0$	ξ	c	n	k	τ	cost
0.05	10	0.2	3.4384	23	3	3.7927	35.6378
		0.4	5.7215	50	5	3.2758	64.1379
		0.6	7.4996	143	6	3.5693	158.1416
		0.8	8.8887	709	10	3.6369	727.6369
	100	0.2	33.0558	25	2	29.6761	41.9352
		0.4	56.6264	54	3	28.4736	74.0421
		0.6	74.8355	148	4	32.1946	172.8778
		0.8	88.8718	715	7	34.0912	752.3638
	1000	0.2	305.9638	39	1	214.6937	70.9694
		0.4	550.7234	72	2	165.1395	116.0279
		0.6	743.3508	176	2	269.0000	240.8000
		0.8	888.0912	760	4	282.7429	885.0971
0.10	10	0.2	3.4404	23	3	3.9401	35.6820
		0.4	5.7273	52	4	3.9062	65.5625
		0.6	7.5003	147	5	4.2044	161.6022
		0.8	8.8888	730	8	4.4530	747.5624
	100	0.2	33.0461	26	2	30.1397	43.0279
		0.4	56.6072	55	3	29.5066	75.3520
		0.6	74.8591	152	3	40.5499	175.6650
		0.8	88.8743	738	5	43.6636	772.3318
	1000	0.2	305.9638	39	1	214.6937	70.9694
		0.4	553.4252	75	1	313.5306	116.8531
		0.6	743.2990	177	2	273.2596	242.6519
		0.8	888.1331	779	3	367.6669	900.8001
0.25	10	0.2	3.4838	24	2	5.1840	36.0368
		0.4	5.7362	55	3	4.9470	67.9841
		0.6	7.5014	155	4	5.3214	169.1286
		0.8	8.8889	774	5	5.9360	789.4680
	100	0.2	33.0214	26	2	31.6344	43.3269
		0.4	56.7697	58	2	41.4984	77.2997
		0.6	74.8997	161	2	54.2004	182.8401
		0.8	88.8751	777	4	56.0377	811.4151
	1000	0.2	305.9638	39	1	214.6937	70.9694
		0.4	553.4252	75	1	313.5306	116.8531
		0.6	744.5997	189	1	486.5533	248.1553
		0.8	888.2246	817	2	513.9998	930.8000

**Table 2.** Optimal acceptance number c and disposition of life test  $(n, k, \tau)$  for  $\alpha = 0.05$  and  $\beta = 0.1$ .

ξ ck τ p n  $\sigma_0$ cost 0.05 10 0.2 3.1761 3 3.9233 33.6770 21 0.4 5.4407 44 4 3.7628 57.5051 0.6 7.2745 120 6 3.6211 135.1726 0.8 8.7678 576 10 3.6599 594.6599 100 0.2 30.5573 24 2 29.7266 40.9453 0.4 53.7769 3 28.0829 67.9249 48 0.6 72.5772 125 4 31.5148 149.6059 0.8 87.6629 585 35.9682 619.5809 6 1000 0.2 284.7215 37 211.9999 68.7000 1 0.4 523.7220 66 2 158.9999 108.8000 0.6 720.8569 152 2 255.0002 214.0000 0.8 875.9995 631 3 335.7142 743.2143 3 0.10 10 4.0777 0.2 3.1781 21 33.7233 0.4 5.4410 4.0090 58.6036 45 4 0.6 4.2773 7.2755 124 5 138.6386 611.5918 8.7679 594 8 4.4898 0.8 2 100 0.2 30.5492 24 30.1910 41.0382 0.4 53.9332 2 39.2473 68.8495 50 40.0223 152.5067 0.6 72.6026 129 3 0.8 87.6639 5 43.1636 635.0818 601 1000 0.2 284.7215 37 1 211.9999 68.7000 0.4 526.0607 68 1 303.7287 108.8729 0.6 720.8091 153 2 259.0001 215.8000 0.8 875.9797 640 3 348.5631 756.0689 0.25 3.2184 2 5.3940 35.0788 10 0.2 23 3 5.4507 5.1022 61.0307 0.4 48 0.6 7.2770 130 4 5.4295 144.1718 0.8 8.7681 630 5 5.9993 645.4997 100 0.2 31.3544 52.2964 41.7296 26 1 0.4 53.9173 2 70.2652 51 41.3261 0.6 72.6475 136 2 54.0773 157.8155 0.8 87.6693 637 3 59.7012 666.4104 1000 0.2 284.7215 37 211.9999 68.7000 1 0.4 526.0607 68 1 303.7287 108.8729 0.6 722.0335 162 1 467.6105 219.2610 493.0002 779.6000 0.8 876.0719 670 2

**Table 3.** Optimal acceptance number c and disposition of life test  $(n, k, \tau)$  for  $\alpha = 0.1$  and  $\beta = 0.05$ .

<u> </u>						= 0.1 and $\rho$	
p	$\sigma_0$	ξ	c	n	k	τ	cost
0.05	10	0.2	3.7176	15	3	3.4046	27.5214
		0.4	6.0364	36	4	3.3969	49.3587
		0.6	7.7371	106	6	3.3988	121.0393
		0.8	9.0129	546	9	3.6386	563.7747
	100	0.2	35.3198	18	2	24.8153	33.9631
		0.4	59.5100	39	3	24.7401	57.9220
		0.6	77.1632	111	4	29.2464	134.6986
		0.8	90.1109	553	6	34.8597	586.9158
	1000	0.2	323.5116	29	1	173.1642	56.8164
		0.4	576.9250	55	2	137.7145	93.5429
		0.6	765.7411	136	2	234.3090	193.8618
		0.8	900.4147	598	3	323.8596	706.6579
0.10	10	0.2	3.7185	16	3	3.5318	28.5595
		0.4	6.0435	38	3	4.1232	50.7369
		0.6	7.7375	109	5	4.0160	123.5080
		0.8	9.0129	563	7	4.4484	579.6138
	100	0.2	35.3030	18	2	25.1894	34.0379
		0.4	59.6639	41	2	34.7155	58.9431
		0.6	77.1848	114	3	37.2190	136.6657
		0.8	90.1114	569	5	41.8568	602.4284
	1000	0.2	323.5116	29	1	173.1642	56.8164
		0.4	579.3679	57	1	263.9999	93.9000
		0.6	765.6887	137	2	237.9998	195.6000
		0.8	900.3934	607	3	336.2160	719.3648
0.25	10	0.2	3.7661	17	2	4.7029	28.9406
		0.4	6.0435	39	3	4.6038	51.8811
		0.6	7.7382	115	4	5.0995	129.0398
		0.8	9.0129	596	5	5.8348	611.4174
	100	0.2	36.2779	20	1	44.1552	34.9155
		0.4	59.6360	42	2	36.5255	60.3051
		0.6	77.2250	120	2	50.4399	141.0880
		0.8	90.1157	603	3	57.9713	631.8914
	1000	0.2	323.5116	29	1	173.1642	56.8164
		0.4	579.3679	57	1	263.9999	93.9000
		0.6	766.9385	144	1	431.0000	197.6000
		0.8	900.4815	635	2	476.3695	741.2739

**Table 4.** Optimal acceptance number c and disposition of life test  $(n, k, \tau)$  for  $\alpha = 0.1$  and  $\beta = 0.1$ .

0.05         10         0.2         3.4146         14         3         3.5139         26.5542           0.4         5.7185         31         4         3.4698         44.3879           0.6         7.4985         88         5         3.7180         102.3590           0.8         8.8886         431         9         3.6551         448.7896           100         0.2         32.4474         16         2         24.6939         31.9388           0.4         56.4934         35         2         33.6457         52.7291           0.6         74.7492         91         4         28.2447         114.2979           0.8         88.8647         437         6         33.9325         470.3595           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5568         115         2         218.9025         169.7805           0.8         887.8703         479         3         302.3580         581.2074           0.10         10         0.2         3.4585	p	$\sigma_0$	ξ	С	n	k	τ	cost
0.6 7.4985 88 5 3.7180 102.3590 0.8 8.8886 431 9 3.6551 448.7896 100 0.2 32.4474 16 2 24.6939 31.9388 0.4 56.4934 35 2 33.6457 52.7291 0.6 74.7492 91 4 28.2447 114.2979 0.8 88.8647 437 6 33.9325 470.3595 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5568 115 2 218.9025 169.7805 0.8 887.8703 479 3 302.3580 581.2074 0.10 10 0.2 3.4585 15 2 4.6419 26.9284 0.4 5.7268 32 3 4.2390 44.7717 0.6 7.4982 89 5 4.0698 103.5349 0.8 8.8886 444 7 4.4802 460.6361 100 0.2 32.4329 17 2 25.0653 33.0131 0.4 56.4845 35 2 34.2003 52.8401 0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.8 88.8871 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000	0.05	10	0.2	3.4146	14	3	3.5139	26.5542
0.8         8.8886         431         9         3.6551         448.7896           100         0.2         32.4474         16         2         24.6939         31.9388           0.4         56.4934         35         2         33.6457         52.7291           0.6         74.7492         91         4         28.2447         114.2979           0.8         88.8647         437         6         33.9325         470.3595           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5568         115         2         218.9025         169.7805           0.8         887.8703         479         3         302.3580         581.2074           0.10         10         0.2         3.4585         15         2         4.6419         26.9284           0.4         5.7268         32         3         4.2390         44.7717         0.6         7.4982         89         5         4.0698         103.5349         0.8         8.8886         444         7         4.4802         460.6361<			0.4	5.7185	31	4	3.4698	44.3879
100         0.2         32.4474         16         2         24.6939         31.9388           0.4         56.4934         35         2         33.6457         52.7291           0.6         74.7492         91         4         28.2447         114.2979           0.8         88.8647         437         6         33.9325         470.3595           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5568         115         2         218.9025         169.7805           0.8         887.8703         479         3         302.3580         581.2074           0.10         10         0.2         3.4585         15         2         4.6419         26.9284           0.4         5.7268         32         3         4.2390         44.7717         44.6098         103.5349           0.8         8.8886         444         7         4.4802         460.6361         460.6361           100         0.2         32.4329         17         2         25.0653         33.0131			0.6	7.4985	88	5	3.7180	102.3590
0.4 56.4934 35 2 33.6457 52.7291 0.6 74.7492 91 4 28.2447 114.2979 0.8 88.8647 437 6 33.9325 470.3595 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5568 115 2 218.9025 169.7805 0.8 887.8703 479 3 302.3580 581.2074 0.10 10 0.2 3.4585 15 2 4.6419 26.9284 0.4 5.7268 32 3 4.2390 44.7717 0.6 7.4982 89 5 4.0698 103.5349 0.8 8.8886 444 7 4.4802 460.6361 100 0.2 32.4329 17 2 25.0653 33.0131 0.4 56.4845 35 2 34.2003 52.8401 0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706			0.8	8.8886	431	9	3.6551	448.7896
0.6 74.7492 91 4 28.2447 114.2979 0.8 88.8647 437 6 33.9325 470.3595 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5568 115 2 218.9025 169.7805 0.8 887.8703 479 3 302.3580 581.2074 0.10 10 0.2 3.4585 15 2 4.6419 26.9284 0.4 5.7268 32 3 4.2390 44.7717 0.6 7.4982 89 5 4.0698 103.5349 0.8 8.8886 444 7 4.4802 460.6361 100 0.2 32.4329 17 2 25.0653 33.0131 0.4 56.4845 35 2 34.2003 52.8401 0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000		100	0.2	32.4474	16	2	24.6939	31.9388
0.8         88.8647         437         6         33.9325         470.3595           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5568         115         2         218.9025         169.7805           0.8         887.8703         479         3         302.3580         581.2074           0.10         10         0.2         3.4585         15         2         4.6419         26.9284           0.4         5.7268         32         3         4.2390         44.7717           0.6         7.4982         89         5         4.0698         103.5349           0.8         8.8886         444         7         4.4802         460.6361           100         0.2         32.4329         17         2         25.0653         33.0131           0.4         56.4845         35         2         34.2003         52.8401           0.6         74.7731         94         3         36.2773         116.3832           0.8         88.8654         449         5			0.4	56.4934	35	2	33.6457	52.7291
1000       0.2       299.1226       27       1       170.0000       54.5000         0.4       548.7136       51       1       252.7058       86.7706         0.6       741.5568       115       2       218.9025       169.7805         0.8       887.8703       479       3       302.3580       581.2074         0.10       10       0.2       3.4585       15       2       4.6419       26.9284         0.4       5.7268       32       3       4.2390       44.7717         0.6       7.4982       89       5       4.0698       103.5349         0.8       8.8886       444       7       4.4802       460.6361         100       0.2       32.4329       17       2       25.0653       33.0131         0.4       56.4845       35       2       34.2003       52.8401         0.6       74.7731       94       3       36.2773       116.3832         0.8       88.8654       449       5       40.9857       481.9929         1000       0.2       299.1226       27       1       170.0000       54.5000         0.4       5.7274       33       3			0.6	74.7492	91	4	28.2447	114.2979
0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5568         115         2         218.9025         169.7805           0.8         887.8703         479         3         302.3580         581.2074           0.10         10         0.2         3.4585         15         2         4.6419         26.9284           0.4         5.7268         32         3         4.2390         44.7717           0.6         7.4982         89         5         4.0698         103.5349           0.8         8.8886         444         7         4.4802         460.6361           100         0.2         32.4329         17         2         25.0653         33.0131           0.4         56.4845         35         2         34.2003         52.8401           0.6         74.7731         94         3         36.2773         116.3832           0.8         88.8654         449         5         40.9857         481.9929           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         5.7274         33         3			0.8	88.8647	437	6	33.9325	470.3595
0.6 741.5568 115 2 218.9025 169.7805 0.8 887.8703 479 3 302.3580 581.2074 0.10 10 0.2 3.4585 15 2 4.6419 26.9284 0.4 5.7268 32 3 4.2390 44.7717 0.6 7.4982 89 5 4.0698 103.5349 0.8 8.8886 444 7 4.4802 460.6361 100 0.2 32.4329 17 2 25.0653 33.0131 0.4 56.4845 35 2 34.2003 52.8401 0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000		1000	0.2	299.1226	27	1	170.0000	54.5000
0.8         887.8703         479         3         302.3580         581.2074           0.10         10         0.2         3.4585         15         2         4.6419         26.9284           0.4         5.7268         32         3         4.2390         44.7717           0.6         7.4982         89         5         4.0698         103.5349           0.8         8.8886         444         7         4.4802         460.6361           100         0.2         32.4329         17         2         25.0653         33.0131           0.4         56.4845         35         2         34.2003         52.8401           0.6         74.7731         94         3         36.2773         116.3832           0.8         88.8654         449         5         40.9857         481.9929           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5042         116         2         222.2136         171.4427           0.8         887.9672         495         2			0.4	548.7136	51	1	252.7058	86.7706
0.10         10         0.2         3.4585         15         2         4.6419         26.9284           0.4         5.7268         32         3         4.2390         44.7717           0.6         7.4982         89         5         4.0698         103.5349           0.8         8.8886         444         7         4.4802         460.6361           100         0.2         32.4329         17         2         25.0653         33.0131           0.4         56.4845         35         2         34.2003         52.8401           0.6         74.7731         94         3         36.2773         116.3832           0.8         88.8654         449         5         40.9857         481.9929           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         741.5042         116         2         222.2136         171.4427           0.8         887.9672         495         2         426.9999         591.4000           0.25         10         0.2         3.4618			0.6	741.5568	115	2	218.9025	169.7805
0.4       5.7268       32       3       4.2390       44.7717         0.6       7.4982       89       5       4.0698       103.5349         0.8       8.8886       444       7       4.4802       460.6361         100       0.2       32.4329       17       2       25.0653       33.0131         0.4       56.4845       35       2       34.2003       52.8401         0.6       74.7731       94       3       36.2773       116.3832         0.8       88.8654       449       5       40.9857       481.9929         1000       0.2       299.1226       27       1       170.0000       54.5000         0.4       548.7136       51       1       252.7058       86.7706         0.6       741.5042       116       2       222.2136       171.4427         0.8       887.9672       495       2       426.9999       591.4000         0.25       10       0.2       3.4618       15       2       4.8953       26.9791         0.4       5.7274       33       3       4.7361       45.9208         0.6       7.5010       95       3       5.5153 </th <th></th> <th></th> <th>0.8</th> <th>887.8703</th> <th>479</th> <th>3</th> <th>302.3580</th> <th>581.2074</th>			0.8	887.8703	479	3	302.3580	581.2074
0.6 7.4982 89 5 4.0698 103.5349 0.8 8.8886 444 7 4.4802 460.6361 100 0.2 32.4329 17 2 25.0653 33.0131 0.4 56.4845 35 2 34.2003 52.8401 0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000	0.10	10	0.2	3.4585	15	2	4.6419	26.9284
0.8       8.8886       444       7       4.4802       460.6361         100       0.2       32.4329       17       2       25.0653       33.0131         0.4       56.4845       35       2       34.2003       52.8401         0.6       74.7731       94       3       36.2773       116.3832         0.8       88.8654       449       5       40.9857       481.9929         1000       0.2       299.1226       27       1       170.0000       54.5000         0.4       548.7136       51       1       252.7058       86.7706         0.6       741.5042       116       2       222.2136       171.4427         0.8       887.9672       495       2       426.9999       591.4000         0.25       10       0.2       3.4618       15       2       4.8953       26.9791         0.4       5.7274       33       3       4.7361       45.9208         0.6       7.5010       95       3       5.5153       108.1546         0.8       8.8887       470       5       5.8908       485.4454         100       0.2       33.3131       18       1 </th <th></th> <th></th> <th>0.4</th> <th>5.7268</th> <th>32</th> <th>3</th> <th>4.2390</th> <th>44.7717</th>			0.4	5.7268	32	3	4.2390	44.7717
100       0.2       32.4329       17       2       25.0653       33.0131         0.4       56.4845       35       2       34.2003       52.8401         0.6       74.7731       94       3       36.2773       116.3832         0.8       88.8654       449       5       40.9857       481.9929         1000       0.2       299.1226       27       1       170.0000       54.5000         0.4       548.7136       51       1       252.7058       86.7706         0.6       741.5042       116       2       222.2136       171.4427         0.8       887.9672       495       2       426.9999       591.4000         0.25       10       0.2       3.4618       15       2       4.8953       26.9791         0.4       5.7274       33       3       4.7361       45.9208         0.6       7.5010       95       3       5.5153       108.1546         0.8       8.8887       470       5       5.8908       485.4454         100       0.2       33.3131       18       1       44.5089       32.9509         0.4       56.4580       36       2 </th <th></th> <th></th> <th>0.6</th> <th>7.4982</th> <th>89</th> <th>5</th> <th>4.0698</th> <th>103.5349</th>			0.6	7.4982	89	5	4.0698	103.5349
0.4 56.4845 35 2 34.2003 52.8401 0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.8	8.8886	444	7	4.4802	460.6361
0.6 74.7731 94 3 36.2773 116.3832 0.8 88.8654 449 5 40.9857 481.9929 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000		100	0.2	32.4329	17	2	25.0653	33.0131
0.8       88.8654       449       5       40.9857       481.9929         1000       0.2       299.1226       27       1       170.0000       54.5000         0.4       548.7136       51       1       252.7058       86.7706         0.6       741.5042       116       2       222.2136       171.4427         0.8       887.9672       495       2       426.9999       591.4000         0.25       10       0.2       3.4618       15       2       4.8953       26.9791         0.4       5.7274       33       3       4.7361       45.9208         0.6       7.5010       95       3       5.5153       108.1546         0.8       8.8887       470       5       5.8908       485.4454         100       0.2       33.3131       18       1       44.5089       32.9509         0.4       56.4580       36       2       35.9718       54.1944         0.6       74.8192       99       2       49.8122       119.9624         0.8       88.8712       476       3       57.5479       504.7644         1000       0.2       299.1226       27 <td< th=""><th></th><th></th><th>0.4</th><th>56.4845</th><th>35</th><th>2</th><th>34.2003</th><th>52.8401</th></td<>			0.4	56.4845	35	2	34.2003	52.8401
1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.6	74.7731	94	3	36.2773	116.3832
0.4 548.7136 51 1 252.7058 86.7706 0.6 741.5042 116 2 222.2136 171.4427 0.8 887.9672 495 2 426.9999 591.4000 0.25 10 0.2 3.4618 15 2 4.8953 26.9791 0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.8	88.8654	449	5	40.9857	481.9929
0.6     741.5042     116     2     222.2136     171.4427       0.8     887.9672     495     2     426.9999     591.4000       0.25     10     0.2     3.4618     15     2     4.8953     26.9791       0.4     5.7274     33     3     4.7361     45.9208       0.6     7.5010     95     3     5.5153     108.1546       0.8     8.8887     470     5     5.8908     485.4454       100     0.2     33.3131     18     1     44.5089     32.9509       0.4     56.4580     36     2     35.9718     54.1944       0.6     74.8192     99     2     49.8122     119.9624       0.8     88.8712     476     3     57.5479     504.7644       1000     0.2     299.1226     27     1     170.0000     54.5000       0.4     548.7136     51     1     252.7058     86.7706       0.6     742.6893     121     1     407.9999     172.3000		1000	0.2	299.1226	27	1	170.0000	54.5000
0.8         887.9672         495         2         426.9999         591.4000           0.25         10         0.2         3.4618         15         2         4.8953         26.9791           0.4         5.7274         33         3         4.7361         45.9208           0.6         7.5010         95         3         5.5153         108.1546           0.8         8.8887         470         5         5.8908         485.4454           100         0.2         33.3131         18         1         44.5089         32.9509           0.4         56.4580         36         2         35.9718         54.1944           0.6         74.8192         99         2         49.8122         119.9624           0.8         88.8712         476         3         57.5479         504.7644           1000         0.2         299.1226         27         1         170.0000         54.5000           0.4         548.7136         51         1         252.7058         86.7706           0.6         742.6893         121         1         407.9999         172.3000			0.4	548.7136	51	1	252.7058	86.7706
0.25     10     0.2     3.4618     15     2     4.8953     26.9791       0.4     5.7274     33     3     4.7361     45.9208       0.6     7.5010     95     3     5.5153     108.1546       0.8     8.8887     470     5     5.8908     485.4454       100     0.2     33.3131     18     1     44.5089     32.9509       0.4     56.4580     36     2     35.9718     54.1944       0.6     74.8192     99     2     49.8122     119.9624       0.8     88.8712     476     3     57.5479     504.7644       1000     0.2     299.1226     27     1     170.0000     54.5000       0.4     548.7136     51     1     252.7058     86.7706       0.6     742.6893     121     1     407.9999     172.3000			0.6	741.5042	116	2	222.2136	171.4427
0.4 5.7274 33 3 4.7361 45.9208 0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.8	887.9672	495	2	426.9999	591.4000
0.6 7.5010 95 3 5.5153 108.1546 0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000	0.25	10	0.2	3.4618	15	2	4.8953	26.9791
0.8 8.8887 470 5 5.8908 485.4454 100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.4	5.7274	33	3	4.7361	45.9208
100 0.2 33.3131 18 1 44.5089 32.9509 0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.6	7.5010	95	3	5.5153	108.1546
0.4 56.4580 36 2 35.9718 54.1944 0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.8	8.8887	470	5	5.8908	485.4454
0.6 74.8192 99 2 49.8122 119.9624 0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000		100	0.2	33.3131	18	1	44.5089	32.9509
0.8 88.8712 476 3 57.5479 504.7644 1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.4	56.4580	36	2	35.9718	54.1944
1000 0.2 299.1226 27 1 170.0000 54.5000 0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.6	74.8192	99	2	49.8122	119.9624
0.4 548.7136 51 1 252.7058 86.7706 0.6 742.6893 121 1 407.9999 172.3000			0.8	88.8712	476	3	57.5479	504.7644
0.6 742.6893 121 1 407.9999 172.3000		1000	0.2	299.1226	27	1	170.0000	54.5000
			0.4	548.7136	51	1	252.7058	86.7706
1			0.6	742.6893	121	1	407.9999	172.3000
0.8 887.9371 506 2 450.0002 607.0000			0.8	887.9371	506	2	450.0002	607.0000

ability requirement by consumers, so it is agreed with intuition. The design parameters do not vary much according to different values of p when the other conditions remain unchanged. When the value of  $\sigma_0$  increases, the sample size increases but the number of inspections decreases. When the consumer's risk or the producer's risk increases, the total cost tends to decrease.

Further, we compare the design parameters and cost for fixed value of  $\alpha = 0.05$  and two values of  $\beta =$ 0.05 and  $\beta = 0.01$  for p = 0.1 and  $\sigma_0 = 100$  from Table 1 and Table 2. We presented these design parameters along with the cost in Table 5. From Table 5 we can see that for other fixed values as  $\beta$  increases from 0.05 to 0.1, the values of c, n and cost decreases.

We noted the same trend in design parameters and cost when  $\alpha$  decreasing from 0.05 to 0.01 (Table 3~ Table 4) and same values of  $\beta$ .

**Example 1:** Suppose that the quality engineer wants to use the proposed reliability sampling plan for a particular lot of products. The lifetime of the products follows a Pareto distribution of second kind with shape parameter  $\lambda = 1$  and scale parameter  $\sigma$ . Because  $\sigma$  is the median life, large value of  $\sigma$  is desirable to the engineer (or producer) as well as the consumer. The producer's risk is specified by 0.05 if the true median life is as large as  $\sigma_0 = 100$  and the consumer's risk is specified by 0.05 if the true median life is as low as  $\sigma_1$  = 60. Consider a progressive type-I interval censoring with removal probability p = 0.1 and cost parameters  $C_a = \$10$ ,  $C_s = \$1$ ,  $C_i = \$0.5$ ,  $C_o = \$0.1$ . From Table 1, the parameters are obtained by: n = 152, k = 3,  $\tau = 40.5499$  and c = 74.8591 Therefore, the engineer needs to draw a random sample with size n = 152 from the lot and put them on a 3-stage progressive type-I interval censored life test with constant inspection length t = 40.5499. Suppose now that we obtain the failure data as  $n_1 = 46$ ,  $n_2 = 17$ ,  $n_3 = 14$ . Then, the number of items removed at each inspection is determined by:  $r_1$ =  $0.1(152-46) \approx 1$ ,  $r_2 = 0.1(95-17) \approx 8$  and  $r_3 = 70-14 =$ 56. The MLE  $\hat{\sigma} = 100.5548$  is obtained from (12). As it is greater than the acceptance number c = 74.8591, therefore the engineer should accept the lot. The total cost required for this test is 175.665.

**Table 5.** Comparison of Plan Parameters and Cost when  $\alpha = 0.05$ , p = 0.1 and  $\sigma_0 = 100$ .

		0.05		$\beta = 0.1$						
Ĕ	С	n	k	τ	cost	С	n	k	τ	cost
0.2	33.0461	26	2	30.1397	43.0279	30.5492	24	2	30.1910	41.0382
0.4	56.6072	55	3	29.5066	75.3520	53.9332	50	2	39.2473	68.8495
0.6	74.8591	152	3	40.5499	175.6650	72.6026	129	3	40.0223	152.5067
0.8	88.8743	738	5	43.6636	772.3318	87.6639	601	5	43.1636	635.0818

## 4. CONCLUDING REMARKS

In the paper, the Pareto distribution of the second kind is considered as a life distribution when designing the acceptance sampling plan based on the progressively type-1 interval censoring scheme. As the Pareto distribution of second kind is skewed distribution, we use the median life as reliability measure. The decision upon the acceptance of lots is based on the MLE of the median life. The cost model is considered and the cost minimization is formulated so as to determine the design parameters such as the sample size, number of inspections and the inspection interval.

As stated in Huang and Wu (2008), one should be cautious in using this sampling plan when the sample size is small because design parameters are derived from the asymptotic distribution. The extension of the present study to some other distributions such as the gamma or the generalized Rayleigh distribution may be possible area for future research.

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