

Investigation of Frequency Dependent Sensitivity of Noise Figure on Device Parameters in 65 nm CMOS

MinSuk Koo, Hakchul Jung, HeeSauk Jhon, Byung-Gook Park, Jong Duk Lee, and Hyungcheol Shin

Abstract—We have investigated the noise sensitivity of low noise amplifier (LNA) at different frequency. This noise sensitivity analysis provides insights about noise parameters and it is very beneficial for making appropriate design trade-offs. From this work, the circuit designer can choose the adequate noise parameters tolerances.

Index Terms—Noise sensitivity, CMOS, low noise amplifier, LNA, optimization

I. INTRODUCTION

RF circuit design is difficult in advanced technology because of process variability and lack of accuracy of model. Therefore, we should take such unpredictable process variations into account during the circuit design stage in deep submicron technology. Noise sensitivity analysis could provide the design approach to reduce these variations for better circuit design. A low-noise Amplifier (LNA) is one of the most critical circuit blocks in a wireless transceiver. As the first stage in the receiver architecture, noise figure of LNA dominates overall noise performance of the system [1]. Therefore, we analyzed frequency dependent sensitivity of noise figure of LNA. For more accuracy, we adopted small signal equivalent circuit with gate-to-drain capacitance consideration and analytic noise model of MOSFET. This work is done by measurement data of 65 nm CMOS devices.

Manuscript received Mar. 2, 2009; revised Mar. 11, 2009.
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II. NOISE FIGURE OF LNAs

Conventional LNAs schematic is shown in Fig. 1. And small signal equivalent circuit with C_{gd} is shown in Fig. 2.

As the technology is scaled down, the effect of the C_{gd} is not ignored any more. From that equivalent circuit, noise figure equation can be derived as below [2]. The channel thermal noise, S_{id} , is analytically modeled and predicts the measured channel thermal noise well [3,4].

$$NF-1 = \frac{R_l}{R_s} + \frac{S_{id1}}{4kT} \frac{(R_s + R_l)^2}{R_s} \left(\frac{f}{f_{T1}}\right)^2 + \frac{S_{id2}}{4kT} (4R_s) \left(\frac{f}{f_{T1}}\right)^2 \left(\frac{f}{f_{T2}}\right)^2 \quad (1)$$

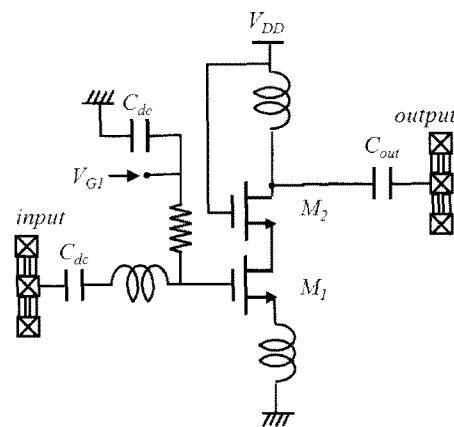


Fig. 1. Schematic of a conventional cascode LNA.

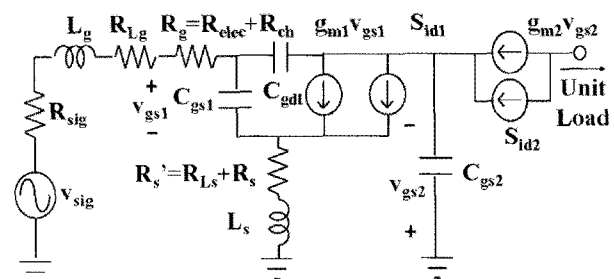


Fig. 2. Small signal equivalent circuit of cascode LNA with C_{gd} .

$$NF - 1 = \frac{R_1}{R_{sig}} + 4R_{sig} \frac{\alpha S_{id1}}{\gamma 4kT} + 4R_{sig} \frac{\beta S_{id2}}{\gamma 4kT} \quad (2)$$

$$S_{id} = 4kT_0 \left(\frac{m}{(V_{GT} - V_0)} + \frac{mV_0}{V_{GT}(V_{GT} - V_0)} \right) I_D \quad (3)$$

where $V_{GT} = V_{GS} - V_{TH}$, $V_0 = I_{DS} / WC_{ox} v_{sat}$, and m is the body-effect coefficient. R_1 is sum of parasitic resistance of gate and source inductor (R_{Lg} , R_s), gate electrode resistance (R_{elec}) and source resistance (R_s). The equation (1) is extended to equation (2) with C_{gd} consideration. And parameters such as α , β and γ are as shown below where $C_{gs}' = C_{gs1} + C_{gs2}$ and $R_{tot} = R_1 + R_{sig}$ [2].

$$\alpha = \frac{\left[\left(1 + \frac{C_{gd1}}{C_{gs1}} \right) R_{tot} \right]^2}{\left[\frac{g_{m1} L_s + R_{tot}}{C_{gs1}} + \frac{C_{gd1}}{C_{gs1}} \left(1 + \frac{g_{m1}}{g_{m2}} \right) R_{tot} \right]^2 + \left[\omega L_s \left(1 + \frac{C_{gd1}}{C_{gs1}} g_{m1} R_{tot} \right) + \frac{\omega}{g_{m2}} \left(C_{gs2} \left(\frac{g_{m1} L_s}{C_{gs1}} + R_{tot} \right) + \frac{C_{gd1}}{C_{gs1}} (g_{m1} (L_g + L_s)) \right) \right]^2} \quad (4)$$

$$\beta = \frac{\left(-\omega C_{gs2} \left(-\frac{1}{\omega C_{gs1}} + \omega L_g \right) + \omega C_{gd1} \left(\frac{g_{m1} R_{tot}}{\omega C_{gs1}} \right) \right)^2 + \omega^2 \left(C_{gs2} \left(\frac{g_{m1} L_s}{C_{gs1}} + R_{tot} \right) + \frac{C_{gd1}}{C_{gs1}} (g_{m1} L_g + C_{gs}' R_{tot}) \right)^2}{\left(-\omega C_{gs2} \left(-\frac{1}{\omega C_{gs1}} + \omega L_g \right) + g_{m2} \left(\frac{g_{m1} L_s}{C_{gs1}} + R_{tot} \right) \right)^2 + \frac{C_{gd1}}{C_{gs1}} \left(\frac{1 - \omega^2 g_{m1} g_{m2} L_g L_s + (g_{m1} + g_{m2}) R_{tot}}{-\omega^2 L_g C_{gs}'} \right)} \quad (5)$$

$$\gamma = \left(\frac{g_{m1}}{\omega [C_{gs1} + C_{gd1} \left(1 + \frac{g_{m1}}{g_{m2}} \right)]} \right)^2 \quad (6)$$

There are two noise terms with different noise sources; resistor source and transistor source [4]. Therefore, we could classify parameters as two noise sources. Q-factor and L_g are related to resistor noise term and V_{th} , width of device, C_{ox} , v_{sat} and drain current are related to transistor noise term. And other parameters such as C_{gs} , C_{gd} , g_m are multiplied with noise terms. Since there are dominant noise terms at different frequency, we could obtain the sensitivity of these parameters. As frequency increases, $1/\omega^2 C_{gs}$ decreases and L_g , L_s and its parasitic resistance get smaller. Therefore, resistor noise term decreases while the transistor noise term increase as f/f_t increases in simplified noise figure equation (1). As a result, parameters related to transistor noise term would be more sensitive

than others at high frequency while parameters related to resistor noise term are more sensitive at low frequency [5].

III. OPTIMIZATION WITH FOM AND SENSITIVITY ANALYSIS

At higher frequency, we generally use smaller device width. Since the noise sensitivity varies as width of device changes, we should first determine the optimum width of device and bias point of LNA for more similarity to real design situation. The figure of merit (FoM) represented as below is index of performance of LNA [6].

$$FoM_{LNA} = \frac{G \cdot f}{(NF - 1) \cdot P} \quad (7)$$

where G is signal power gain in absolute unit, NF is noise factor in absolute unit, P is power dissipation, and f is operation frequency. We can obtain the FoM of LNA using following gain equation and FoM optimization for 17 GHz is shown as Fig. 3-(a), (b) where f_{T1} and f_{T2} are cut-off frequency of M_1 and M_2 transistor.

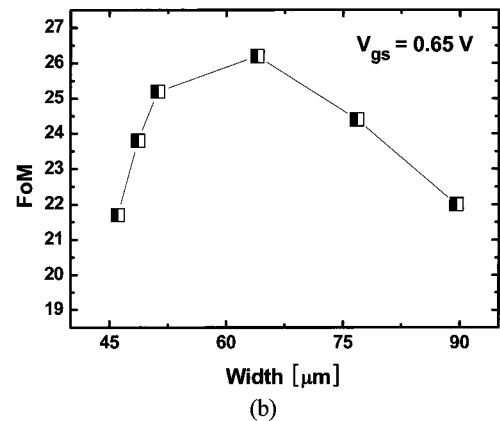
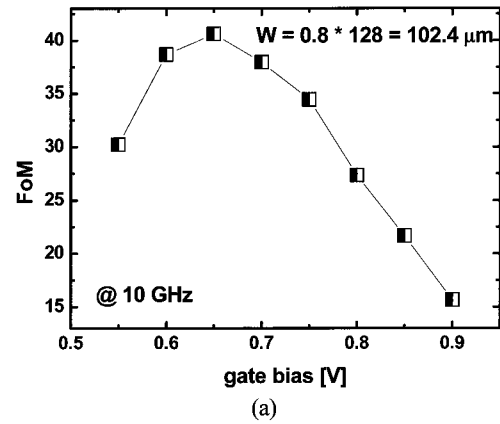
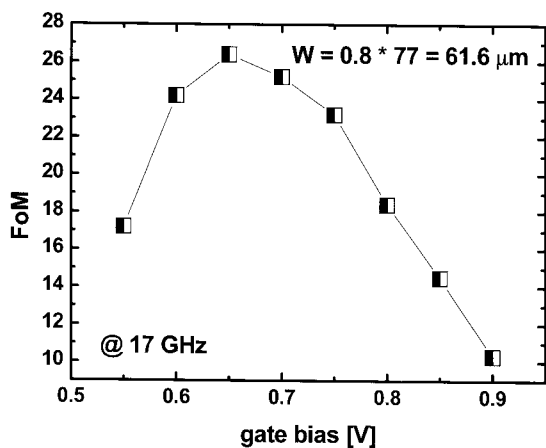
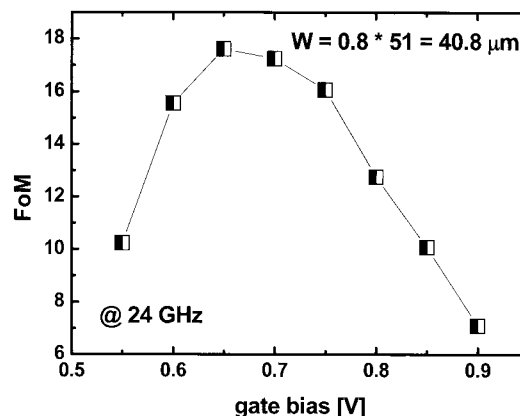


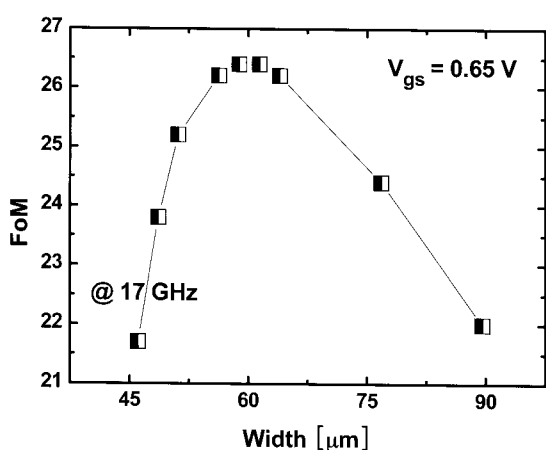
Fig. 3-1. FoM Optimization of LNAs (a) width optimization and (b) gate bias optimization for 10 GHz.



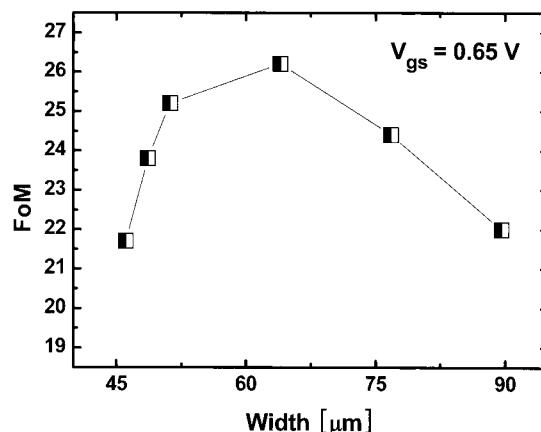
(a)



(a)



(b)



(b)

Fig. 3-2. FoM Optimization of LNAs (a) width optimization and (b) gate bias optimization for 17 GHz.

Fig. 3-3. FoM Optimization of LNAs (a) width optimization and (b) gate bias optimization for 24 GHz.

$$G = \frac{1}{4} \left(\frac{f_{T1}}{f} \right)^2 / \left(1 + \left(\frac{f}{f_{T2}} \right)^2 \right) \quad (8)$$

We can also obtain the FoM of LNA for 10 GHz and 24 GHz for comparison. Optimum device width of 102.4 μm for 10 GHz, 61.6 μm for 17 GHz and 40.8 μm for 24 GHz were obtained at $V_{gs} = 0.65$ V. Fig. 4 shows the effect of S_{id} on noise figure. The $\pm 50\%$ variation of S_{id1} makes deviation of 0.35 dB at 10 GHz, 0.56 dB at 17 GHz, 0.76 dB at 24 GHz. At higher frequency, channel thermal noise is sensitive on noise figure and S_{id1} is more sensitive than S_{id2} for all frequency range. However, the effect of S_{id2} on noise figure is increased more rapidly than that of S_{id1} .

To invest frequency dependent sensitivity of other design parameters, all parameters have been changed by 10% from the nominal value and see the variation of total noise figure.

Fig. 5-(a), (b), (c) shows deviations of noise figure by

10% of change of each parameter. Gate inductor, Q factor, C_{gs1} , C_{gd1} , C_{gs2} , g_{m1} and g_{m2} are considered as important parameters on noise figure.

The nominal values of noise figure are 1.96 dB at 10 GHz, 2.5 dB at 17 GHz, 3.58 dB at 24 GHz. These results provide which parameter should be considered firstly for noise tolerable design.

As we expected, parameters related to resistor noise term such as L_g and Q-factor are more sensitive at lower frequency. And parameters multiplied with noise terms such as C_{gs} , C_{gd} and g_m are more sensitive at higher frequency.

From these results, it is found that parameters which are extracted from DC model such as V_{th} , I_D and g_m are important for all frequency and should be modeled carefully for accurate noise expectation. And parameters related to resistor noise term are important at low frequency while parameters multiplied with transistor noise term are important at high frequency.

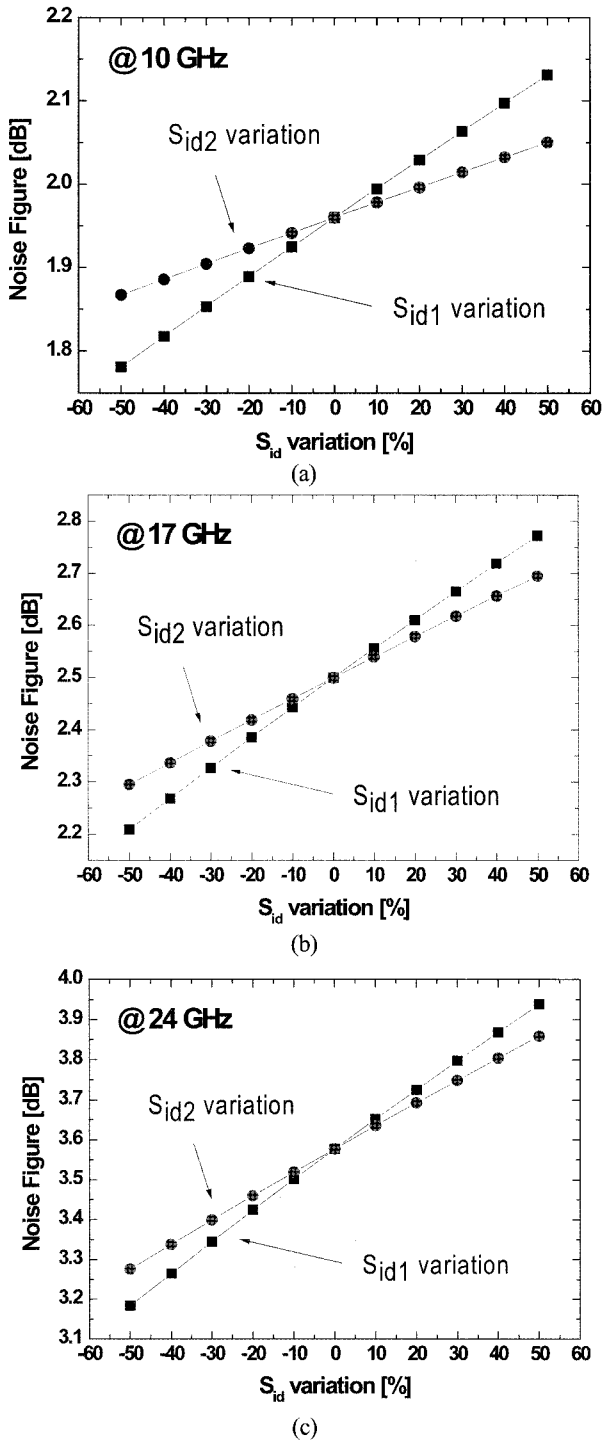


Fig. 4. NF deviation vs. parameters for S_{id} at (a) 10 GHz, (b) 17 GHz and (c) 24 GHz.

IV. CONCLUSIONS

In this paper, we designed LNA with FoM optimization and analyze noise sensitivity of LNAs for frequency. Parameters extracted from DC model such as V_{th} , I_D and g_m should be accurate to reduce the unpredictable variation

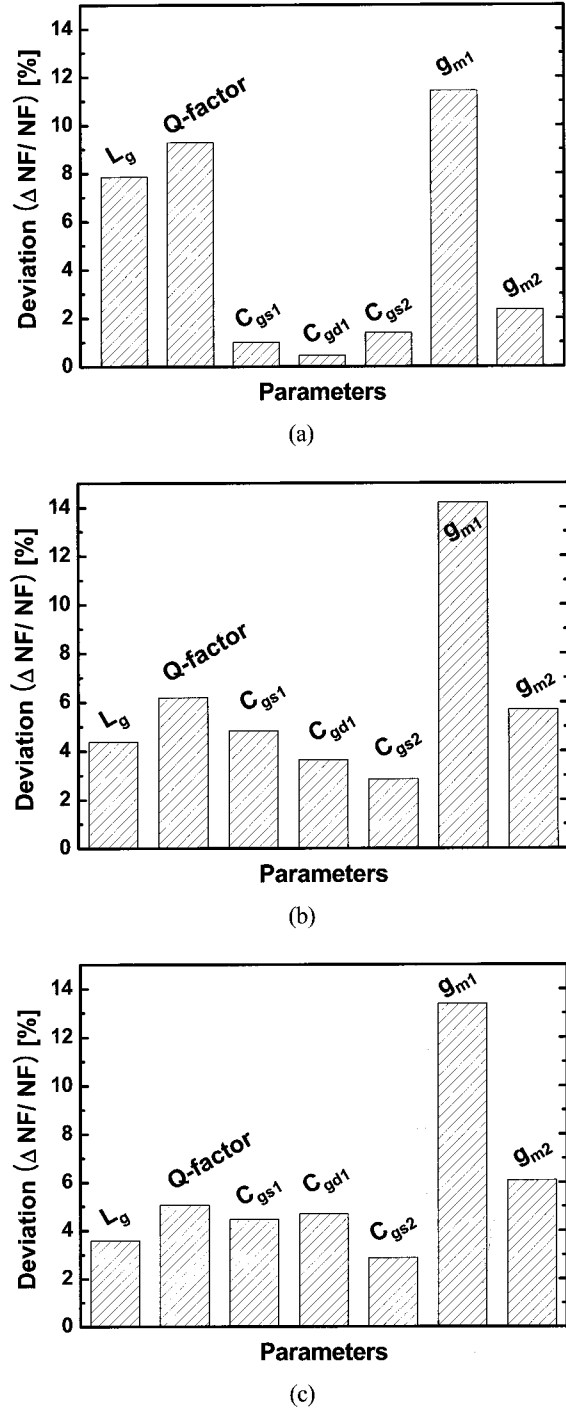


Fig. 5. NF deviation versus parameters for (a) 10GHz, (b) 17GHz and (c) 24 GHz.

for all frequency. And parameters related to resistor noise term are more sensitive at low frequency while parameters multiplied with transistor noise term are more sensitive at high frequency. From this work, circuit designers can determine which parameters are important and focused on. In addition, parasitics which effect on important parameter should be considered firstly.

ACKNOWLEDGMENTS

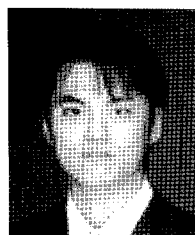
This work was supported by Samsung Electronics Ltd., and Inter-University Semiconductor Research Center (ISRC).

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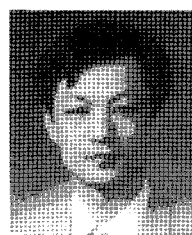
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