# A Study on the Pit Excavation Volume Using Cubic B-Spline

#### **DU-YEOUL MUN\***

\*Deptartment of Civil Engineering, Dongeui University, Busan, Korea

KEY WORDS: Pit-Excavation Volume 토곡량, Spline 스플라인, B-Spline B-스플라인, Spline Surface 스플라인 곡면

요 약: 항만공사같은 대규모의 매립공사에서 토공작업은 총공사비의 상당한 비중을 차지하므로 경제적인 시공을 위하여 切・盛上값은 정확하게 계산되어야 한다. 따라서 본 연구는 주어진 3차원 표고테이터를 지나는 스플라인 곡면을 구하는 알고리 증을 제시함으로써 좀더 정확한 토공량 계산식의 결정을 목표로 한다. 스플라인에 대한 흥미로운 수학적 결과는 무척 많지만 본연구에서는 스플라인 곡면을 기술하고 또 그것을 이용하여 토공량 계산을 위한 알고리즘개발을 목표로 하기 때문에 알고리즘과 프로그래밍에 필요한 수학적 내용을 기술하며 그 수치적 계산결과는 Maple 프로그램을 이용하였다. 그리고 정확도를 비교하기 위하여 기존의 방법인 선형점고법, Chamber법, Chen과 Lin의 이론을 컴퓨터프로그램하여 본 연구에서 제시된 방법과 정확도를 비교 분석한다. 아울러 각 이론식의 결과에 대한 보다 정확한 검사를 위하여 x, y 함수식을 이용한 실험지형을 인위적으로 만들었으며 그 때의 값을 기준값으로 하였다. 따라서 실험수치지형에 대한 기준값이 절대값에 가까우므로 각 토공량식들의 오차규명을 보다 명확하고 확실하게 비교할 수 있도록 하였다.

#### 1. Introduction

Surveyors are often called upon to measure volumes of earthwork needed to be moved for construction of seashore reclamation, highways, railroads, canals, earth dams, pipelines, and similar projects. Earthwork quantities in the types of construction projects described herein are frequently of such magnitude as to make up appreciable percentages of the total project cost. Several methods have been developed for estimating the pit excavation volume ranging from a simple formula to more complicated formulas and numerical methods. The standard methods can be characterized with three basic ideas such as trapezoidal rule, Simpson rule and cubic spline function. The trapezoidal method, which is the most simple method, approximates the ground profile of each grid cell by a plane and estimates the pit excavation volume as the product of the area of the grid cell and the average excavation heights of the grid cell corners (Anderson et al, 1985; Schmidt and Wong, 1985; Wolf and Brinker, 1989; Moffit and Bossler, 1998). This method is the most in common, but the interfaces between approximating planes are sharp and it may not properly describe the ground surface. The Simpson based methods improve the accuracy of the volume estimation for the approximation of the ground surface by considering a second-degree polynomial or a third-degree polyno-mial in each direction of the grid (Easa, 1988; Chambers, 1989). In

Easa (1988), it was 1.assumed that the rectangles formed by the grid were of equal size-that is, the grid was formed by taking equal size intervals along each of the axes. Chambers (1989) generalized Easa's result by allowing grids in which the rectangles were of unequal sizes-that is, the grid were formed by partitioning the axes into intervals of unequal sizes. But both methods have a common drawback: the interfaces of the approximating surfaces are sharp. To eliminate this drawback, Chen and Lin (1991) proposed the cubic spline method, which provides smooth connections between the approximating cubic spline polynomials with the natural boundary conditions. Also, Easa(1998) developed the cubic Hermite polynomial method, which guarantees smooth connections between the approximating cubic Hermite polynomials. In this paper, we propose a method of finding a cubic spline surface, which interpolates the given three dimensional data, by using cubic B-splines. Note that our developed method is different from Chen and Lin's result. Chen and Lin (1991) approximate the ground surface with the cubic spline along one direction and with the linear function along the other direction. But our proposed method approximates the ground surface with the cubic spline polynomial along both x and y directions. The method is based on the cubic B-spline, and the interpolating cubic spline surface can be obtained by those B-splines. Computational results of the proposed method and some comments are presented in section 4. And I have compared the proposed method with the spot height method, line of best fit method, the Chen and Lin method to earthwork volume.

제1저자 문두열 연락처: 부산광역시 부산진구 가야동 산24번지 051-890-1635 dymun@dongeui.ac.kr 20 Du-Yeoul Mun

# 2. Methods of Pit Excavation Volume

#### 2.1 Spot height method

Consider the rectangular grid of whose sides into m and n intervals. The excavation depths f(xi,yi) at the intersection points f(xi,yi), with  $i=0,1,\cdots$ , m and  $j=0,1,\cdots$ , n are known. Then, the composite formular for calculating the volume of total grid, V, is given by

$$V = \frac{h^2}{4} \sum_{i=0}^{m} \sum_{j=0}^{n} a_{ij} f_{ij} \tag{1}$$

in which aij = the corresponding elements of the following matrix

$$a_{ij} = \begin{bmatrix} 1 & 2 & \cdots & 2 & 1 \\ 2 & 1 & \cdots & 4 & 2 \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 2 & 4 & \cdots & 4 & 2 \\ 1 & 2 & \cdots & 2 & 1 \end{bmatrix}$$
 (2)

#### 2.2 Line of best fit method

In this method, a simplified cross section is formed by fitting a straight line to predetermined cross section points using the theory of least squares (see equa. 3).

$$a = \frac{n \sum_{i=1}^{n} x_{i} y_{i} - \sum_{i=1}^{n} x_{i} \sum_{i=1}^{n} y_{i}}{n \sum_{i=1}^{n} x_{i}^{2} - \left(\sum_{i=1}^{n} x_{i}\right)^{2}}$$
(3)

$$b = \frac{-\sum_{i=1}^{n} x_{i} \sum_{i=1}^{n} x_{i} y_{i} + \sum_{i=1}^{n} x_{i}^{2} \sum_{i=1}^{n} y_{i}}{n \sum_{i=1}^{n} x_{i}^{2} - (\sum_{i=1}^{n} x_{i})^{2}}$$
(4)

Value of parameters a and b in Eqs.(3), (4) and vary from one cross section to another due to the variation in elevations.

## 2.3 Chen and Lin method

Considering the area between the x-axis and curve ab, the cubic spline polynomial Sj(x) in the interval(xj, xj+1) may be written in the form

$$S_{j}(x) = a_{j} + b_{j}(x - x_{j}) - c_{j}(x - x_{j})^{2} + d_{j}(x - x_{j})^{3}$$
(5)

and the area Aj can be computed with the integral

$$A_{j} = (a_{j} - b_{j} c_{j} + c_{j} x_{j}^{2} - d_{j} x_{j}^{3})(x_{j+1} - x_{j}) + (\frac{b_{j}}{2} - c_{j} x_{j} - \frac{3 d_{j} x_{j}^{2}}{2})(x_{j+1}^{2} - x_{j}^{2}) + (\frac{c_{j}}{3} - d_{j} x_{j})(d_{j+1}^{3} - x_{j}^{3}) + \frac{d_{j}}{4}(x_{j+1}^{4} - x_{j}^{4})$$
(6)

Using Eq. 6, we can compute the area between the curve ab and the x-axis in the interval  $(x_j, x_j+1)$ , i.e., the area Aj. In

similar manner we can compute the area between the curve ab and the x-axis in the interval (xo, xn) using the following equation:

$$A = \int_{x_0}^{x_n} S(x) dx = \sum_{i=0}^{n-1} A_i$$
 (7)

Eq. 7 is defined as the cubic spline area frmular. we can derive n cubic spline polynomias, Si,0, Si,1,...., Si,n-1 in the x = xi direction.

$$(S_{i,j})_{j=0}^{n-1} = a_{i,j} + b_{i,j}(y - y_j) + c_{i,j}(y - y_j)^2 + d_{i,j}(y - y_j)^3$$
(8)

Using Eq. 6, the formular for calculating the area between the curve that passes through the points f(0,k), f(1,k),..., f(m,k) and the baseline y = yk(z=0) in the interval [(x(0, yk), (x(m, yk))], denoted as Ayk, is given by

$$A_{yk} = \int_{x_0}^{x_1} S_{0,k}(x) dx + \int_{x_1}^{x_2} S_{1,k}(x) dx + \cdots$$

$$+ \int_{x_m}^{x_m} S_{m-1,k}(x) dx$$
 (9)

the points f(0,k), f(1,k),..., f(n,k+1) and the baseline y = yk+1(z=0) in the interval [(x0, yk+1), (xm, yk+1)], denoted as Ayk, is given by

$$A_{yk+1} = \int_{x_0}^{x_1} S_{0,k+1}(x) dx + \int_{x_1}^{x_2} S_{1,k+1}(x) dx + \cdots$$

$$+ \int_{x_0}^{x_m} S_{m-1,k+1}(x) dx$$
 (10)

It is reasonable to use the "end area" method to calculate the excavation volume between Ayk and Ayk+1 as follows:

$$V = \frac{\left(A_{yk} + A_{yk+1}\right) \triangle y}{2} \tag{11}$$

# 2.4 Proposed method(spline surface interpolation and its induced linear systems)

Let two points  $c_1 = (x_1, y_1)$  and  $c_2 = (x_2, y_2)$  be given. Then the line segment joining above two points can be expressed as

$$p(t|c_1, c_2; t_2, t_3) = \frac{t_3 - t}{t_3 - t_2} c_1 + \frac{t - t_2}{t_3 - t_2} c_2, t \in [t_2, t_3]$$
(12)

The two parameters  $t_2$  and  $t_3$  are arbitrary real numbers with  $t_2 \leqslant t_3$ .

If we introduce the piecewise constant functions

$$B_{i,0}(t) = \begin{cases} 1, & t_i \le t < t_{i+1}, \\ 0, & \text{otherwise} \end{cases}$$
 (13)

and set  $p_{i,1}(t) = p(t|c_{i-1}, c_i; t_i, t_{i+1})$ , we can write

$$f(t) = \sum_{i=0}^{n} p_{i,1}(t) B_{i,0}(t)$$
 (14)

For the quadratic spline curve, let three control points  $c_1$ ,  $c_2$ ,  $c_3$  be given and set the knots with  $t_2 \le t_3 < t_4 \le t_5$ . Then we can obtain the quadratic spline curve by using two straight lines passing through  $c_1$  and  $c_2$ ,  $c_2$  and  $c_3$  in the following way.

$$p(t|c_1, c_2, c_3; t_2, t_3, t_4, t_5) = \frac{t_4 - t}{t_4 - t_3} p(t|c_1, c_2; t_2, t_4) + \frac{t - t_3}{t_4 - t_2} p(t|c_2, c_3; t_3, t_5).$$
(15)

Here t is the parameter which is in  $[t_3, t_4]$ . For any n control points  $(c_i)_{i=1}^n$ , we can define the piecewise quadratic spline curve by using the formula (15) and the knot vector  $(t_i)_{i=2}^{n+2}$  with  $t_2 \le t_3 < \cdots < t_{n+1} \le t_{n+2}$ . Set  $p_{i,2}(t) = p(t | c_{i-2}, c_{i-1}, c_i; t_{i-1}, t_i, t_{i+1}, t_{i+2})$ . Then we can write the formula more precisely as

$$f(t) = \sum_{i=3}^{n} p_{i,2}(t) B_{i,0}(t)$$
 (16)

Similarly, we can define the piecewise cubic spline curve.

$$f(t) = \sum_{i=1}^{n} p_{i,3}(t) B_{i,0}(t), \qquad (17)$$

The formulas (14), (16), and (17) can also be written in the form of

$$f(t) = \sum_{i=1}^{n} c_i B_{i,d}(t)$$
 (18)

where  $B_{i,d}(t)$  is given by the recurrence relation

$$B_{i,d}(t) = \frac{t - t_i}{t_{i+d} - t_i} B_{i,d-1}(t) + \frac{t_{i+1+d} - t}{t_{i+1+d} - t_{i+1}}$$
(19)  
$$\times B_{i+1,d-1}(t), \quad d = 1, 2, 3.$$

Here the function  $B_{i,d}$  is called a B-spline of degree d(d=1,2,3) with knots  $\boldsymbol{t_i}$ . The B-spline  $B_{j,d}$  depends only on the knots  $(t_i)_{i=1}^{j+d+1}$ . To understand the nature of B-splines,  $B_{j,d}(t) = B(t|t_j,\cdots,t_{j+d+1})$  is sometimes useful. For example, if  $d \ge 2$  and if we set  $(t_j,\cdots,t_{j+d},t_{j+d+1}) = (a,b,\cdots,c,d)$ , then (19) can be written  $B(t|a,b,\cdots,c,d)(t) = \frac{t-a}{c-a}B(t|a,b,\cdots,c)(t)$ 

$$+\frac{d-t}{d-h}B(t|b,\cdots,c,d)(t). \tag{20}$$

We consider an interpolation problem at a set of gridded data  $(x_i, y_i, f_{ij}) \frac{m_1, m_2}{i=1, j=1}$ , where

$$a = x_1 \langle x_2 \rangle \cdots \langle x_m \rangle = b$$
 and  $c = y_1 \langle y_2 \rangle \cdots \langle y_m \rangle = d$ . For

each i,j, we can think of  $f_{ij}$  as the value of an unknown function f=f(x,y) at the point (x,y). We think of  $S_1$  and  $S_2$  as two univariate piecewise cubic spline spaces  $S_1=\operatorname{span}\{\phi_1,\cdots,\phi_{m_i}\}$  and

 $S_2= \mathrm{span}\,\{\varphi_1,\cdots,\varphi_{m_2}\}$ , where the  $\phi$ 's and  $\varphi$ 's are bases of cubic B-splines for the two spaces. With g in the form  $g(x,y)=\sum_{p=1}^{m_1}\sum_{q=1}^{m_2}c_{p,q}\varphi_q(y)\,\phi_p(x)$ , the above interpolation conditions lead to a set of equations

$$\sum_{k=1}^{m_1} \sum_{\alpha=1}^{m_2} C_{p,q} \varphi_q(y_j) \phi_p(x_i) = f_{ij}$$
 (21)

for all  $i=1,\dots,m_1$  and  $j=1,\dots,m_2$ . This double sum can be split into two sets of simple sums

$$\sum_{b=1}^{m_1} d_{p,j} \phi_p(x_i) = f_{ij} \tag{22}$$

$$\sum_{q=1}^{m_{s}} c_{p,q} \varphi_{q}(y_{j}) = d_{p,j}. \tag{23}$$

We can interpret (22) and (23) as follows:

$$\begin{pmatrix} \phi_{1}(x_{1}) & \phi_{2}(x_{1}) & \cdots & \phi_{m_{1}}(x_{1}) \\ \phi_{1}(x_{2}) & \phi_{2}(x_{2}) & \cdots & \phi_{m_{1}}(x_{2}) \\ \vdots & \vdots & \vdots & \vdots \\ \phi_{1}(x_{m_{1}}) & \phi_{2}(x_{m_{1}}) & \cdots & \phi_{m_{1}}(x_{m_{1}}) \end{pmatrix} \begin{pmatrix} d_{1,j} \\ d_{2,j} \\ \vdots \\ d_{m_{1},j} \end{pmatrix} = \begin{pmatrix} f(x_{1}, y_{j}) \\ f(x_{2}, y_{j}) \\ \vdots \\ f(x_{m_{1}}, y_{j}) \end{pmatrix}$$
(24)

After solving the linear systems (23) and (24), we can determine the control points

$$c_{i,j}$$
 ( $i = 1, 2, \dots, m_1, j = 1, 2, \dots, m_2$ ). Substituting t

control points into 
$$g(x, y) = \sum_{p=1}^{m_1} \sum_{q=1}^{m_2} c_{p,q} \varphi_q(y) \phi_p(x)$$

we find a piecewise cubic spline surface g(x, y) such that  $g(x_i, y_j) = f_{ij}$  for

$$\begin{pmatrix} \varphi_{1}(y_{1}) & \varphi_{2}(y_{1}) & \cdots & \varphi_{m_{2}}(y_{1}) \\ \varphi_{1}(y_{2}) & \varphi_{2}(y_{2}) & \cdots & \varphi_{m_{2}}(y_{2}) \\ \vdots & \vdots & \vdots & \vdots \\ \varphi_{1}(y_{m_{2}}) & \varphi_{2}(y_{m_{2}}) & \cdots & \varphi_{m_{2}}(y_{m_{2}}) \end{pmatrix} \begin{pmatrix} c_{i,1} \\ c_{i,2} \\ \vdots \\ c_{i,m_{2}} \end{pmatrix} = \begin{pmatrix} d_{i,1} \\ d_{i,2} \\ \vdots \\ d_{i,m_{2}} \end{pmatrix}$$
(25)

 $i=1,2,\dots,m_1$  and  $j=1,2,\dots,m_2$ . With this interpolating cubic spline surface g(x,y), we can determine the approximate volume in the following way.

Volume 
$$\simeq \int_{a}^{b} \int_{c}^{d} \sum_{p=1}^{m_{1}} \sum_{q=1}^{m_{2}} c_{p,q} \varphi_{q}(y) \phi_{p}(x) dy dx$$
 (26)

Note that there are many ways to determine an appropriate knot vector satisfying the Shoenberg-Whitney nesting 22 Du-Yeoul Mun

conditions for a piecewise cubic spline surface interpolating the given data. In this paper, we only concentrate on the piecewise cubic spline without boundary conditions and suggest method for the choice of an appropriate knot vector which makes cubic B-splines. We consider nonuniform knot vector, and present some computational results of these two cases in the following section.

# 3. Some Computational Results

We use Maple software to implement our proposed algorithm. We test two examples with several cases given by Chen and Lin (1991), spot height method, line of best fit method(1987). The first example is  $f(x, y) = \sqrt{400 + y^2}/y$  for  $1 \le x \le 121$  and  $1 \le y \le 91$ . There are three cases for the first example:

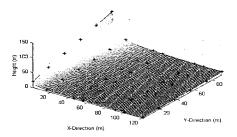


Fig. 1 An example terrain of  $\sqrt{400 + y^2}/y$ 

**Table 1** The height data to case1 of  $\sqrt{400 + y^2}/y$ 

x y	1m	16m	41m	51m	91m	121m
1m	20.02	20.02	20.02	20.02	20.02	20.02
16m	1.60	1.60	1.60	1.60	1.60	1.60
31m	1.19	1.19	1.19	1.19	1.19	1.19
46m	1.09	1.09	1.09	1.09	1.09	1.09
61m	1.05	1.05	1.05	1.05	1.05	1.05
76m	1.03	1.03	1.03	1.03	1.03	1.03
91m	1.02	1.02	1.02	1.02	1.02	1.02

Case 1; a 5 X 6 grid, with unequal intervals [1 16 41 51 91 121] in the x- direction, but with equal intervals [1 16 31 46 61 76 91] in the y- direction, Case 2; a 5 X 6 grid, with equal intervals [1 25 49 73 97 121] in the x-direction, but with unequal intervals [1 11 31 41 71 81 91] in the y-direction,

Case 3; a 5 X 6 grid, with both unequal intervals [1 16 41 51 91 121] in the x-direction and [1 11 31 41 71 81 91] in the y-direction. The second example is  $f(x, y) = (20 + y)/\sqrt{x}$  for  $1 \le x \le 121$  and  $1 \le y \le 91$ . There are three cases for the first example:Case 1; a 6 X 5 grid, with equal intervals [1 21 41 61 81 101 121] in the x-direction, but with unequal intervals [1 26 36 66 81 91] in the y-direction,

**Table 2** The height data to case2 of  $\sqrt{400 + y^2}/y$ 

у	1m	25m	49m	73m	97m	121m
1m	20.02	20.02	20.02	20.02	20.02	20.02
11m	2.08	2.08	2.08	2.08	2.08	2.08
31m	1.19	1.19	1.19	1.19	1.19	1.19
41m	1.11	1.11	1.11	1.11	1.11	1.11
71m	1.04	1.04	1.04	1.04	1.04	1.04
81m	1.03	1.03	1.03	1.03	1.03	1.03
91m	1.02	1.02	1.02	1.02	1.02	1.02

**Table 3** The height data to case3 of  $\sqrt{400 + y^2}/y$ 

y x	1m	16m	41m	51m	91m	121m
1m	20.02	20.02	20.02	20.02	20.02	20.02
11m	2.08	2.08	2.08	2.08	2.08	2.08
31m	1.19	1.19	1.19	1.19	1.19	1.19
41m	1.11	1.11	1.11	1.11	1.11	1.11
71m	1.04	1.04	1.04	1.04	1.04	1.04
81m	1.03	1.03	1.03	1.03	1.03	1.03
91m	1.02	1.02	1.02	1.02	1.02	1.02

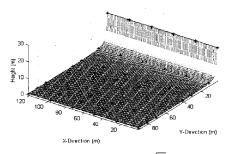


Fig. 2 An example terrain of  $(20 + y)/\sqrt{x}$ 

Case 2; a 6 X 5 grid, with unequal intervals [1 16 46 56 91 101 121] in the x-direction, but with equal intervals [1 19 37 55 73 91] in the y-direction, Case 3; a 5 X 6 grid, with both unequal intervals [1 16 46 56 91 101 121] in the x-direction and [1 26 36 66 81 91] in the y-direction. For the choice of a knot vector satisfying the Schoenberg-Whitney nest conditions, the uniform knot vector is the simplest method.

**Table 4** The height data to case1 of (20 +y)/ $\sqrt{x}$ 

y x	1m	21m	41m	61m	81m	101m	121m
1m	21.00	4.58	3.28	2.69	2.33	2.09	1.91
26m	46.00	2.08	2.08	2.08	2.08	2.08	2.08
36m	56.00	12.22	8.75	7.17	6.22	5.57	5.09
66m	86.00	18.77	13.43	11.01	9.56	8.56	7.82
81m	101.00	22.04	15.77	12.93	11.22	10.05	9.18
91m	111.00	24.22	17.34	14.21	12.33	11.05	10.09

**Table 5** The height data to case2 of  $(20 + y)/\sqrt{x}$ 

y x	1m	16m	46m	56m	91m	101m	121m
1m	21.00	5.25	3.10	2.81	2.20	2.09	1.91
19m	39.00	9.75	5.75	5.21	4.09	3.88	3.55
37m	57.00	14.25	8.40	7.62	5.98	5.67	5.18
55m	75.00	18.75	11.05	10.02	7.86	7.46	6.82
73m	93.00	23.25	13.71	12.43	9.75	9.25	8.45
91m	111.00	27.75	16.37	14.83	11.64	11.05	10.09

**Table 6** The height data to case of  $(20 + y)/\sqrt{x}$ 

y x	1m	16m	46m	56m	91m	101m	121m
1m	21.00	5.25	3.10	2.81	2.20	2.09	1.91
26m	46.00	11.50	6.78	6.15	4.82	4.58	4.18
36m	56.00	14.00	8.26	7.48	5.87	5.57	5.09
66m	86.00	21.50	12.68	11.49	9.02	8.56	7.82
81m	101.00	25.25	14.89	13.50	10.59	10.05	9.18
91m	111.00	27.75	16.37	14.83	11.64	11.05	10.09

Therefore, we test the case of uniform knot vector. We take the uniform knot vector  $[0, 0, 0, 0, \frac{122}{3}, \frac{244}{3}, 122, 122, 122, 122, 122]$  in the x-direction and [0, 0, 0, 0, 23, 46, 69, 92, 92, 92] in the y-direction for the first ex-ample. Also, for the second example, we have the uniform knot vector  $[0, 0, 0, 0, \frac{122}{4}, \frac{244}{4}, \frac{366}{4}, 122, 122, 122, 122]$  in the x-direction and  $[0, 0, 0, 0, \frac{92}{3}, \frac{184}{3}, 92, 92, 92, 92]$  in the,y-direction. For the nonuniform knot vector, we test the first example with [1, 1, 1, 1, 31, 61, 122, 122, 122, 122] in the x-direction and [1, 1, 1, 1, 7, 46, 69, 92, 92, 92, 92] in the y-direction. Also, we test the second example with  $[1, 1, 1, 1, 10, \frac{121}{2}, \frac{363}{4}, 122, 122, 122, 122]$  in the x-direction and  $[1, 1, 1, 1, 1, \frac{91}{3}, \frac{182}{3}, 92, 92, 92, 92]$  in the y-direction. Here we can

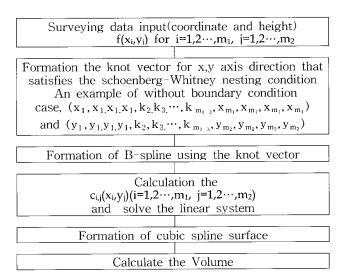


Fig. 3 Flow chart of a proposed method.

**Table** 7 Application results example terrain of  $\sqrt{400 + y^2}/y$ 

	Case	e1	Case	e2	Case3		
Method	Volume (m')	Error (%)	Volume (m')	Error (%)	Volume (m <sup>*</sup> )	Error (%)	
Exact volume	17,109.13	-	17,109.13		17,109.13	-	
Spot	29,664.00	73.381	24,906.00	45.571	24,018.00	40.381	
Line	29817.00	74.280	24519.00	43.310	24519.00	43.310	
Chen	26,178.85	53.011	18,076.02	5.651	18,076.02	5.651	
Proposed	16,945.15	0.960	17,488.18	2.220	17,488.18	2.220	

summarize some computational results. example with [1, 1, 1, 1, 10,  $\frac{121}{2}$ ,  $\frac{363}{4}$ , 122, 122, 122, 122] in the x-direction and [1, 1, 1, 1,  $\frac{91}{3}$   $\frac{182}{3}$ , 92, 92, 92, 92] in the y-direction. Here we can summarize some computational results.

**Table 8** Application results example terrain of  $(20 + y)/\sqrt{x}$ 

	Case1		Case:	2	Case3		
Method	Volume (m')	Error (%)	Volume (m <sup>,</sup> )	Error (%)	Volume (m <sup>3</sup> )	Error (%)	
Exact volume	118,800.00		118,800.00	-	118,800.00	-	
Spot	149,009.30	25.429	141,614.50	19.204	141,613.80	19.204	
Line	178,025.76	49.850	190,359.50	60.240	190,374.40	60.250	
Chen	139,567.80	17.481	122,008.90	2.701	121,859.90	2.576	
Proposed	117,657.45	0.960	119,116.21	0.260	119,116.21	0.260	

Since the ground surface is expressed mathematically, the exact volume can be determined using intergration as  $17,109.13\,\mathrm{m}^3$  and  $118,800\,\mathrm{m}^3$ . From the results of cases 1, 2, 3 of example 1, as shown in Table 7, the error produced using a spot heigt method, line best of fit, Chen and Lin method is  $2.5\sim77$  times larger than that using a proposed method. Similarly, the results of cases 1, 2, 3 of example 2, as shown in Table 8, the error produced using a spot heigt method, line best of fit, Chen and Lin method is  $9.9\sim232$ 

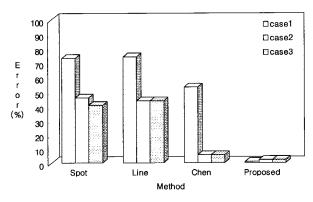


Fig. 4 An earthwork error of the terrain  $\sqrt{400 + y^2}/y$ 

24 Du-Yeoul Mun

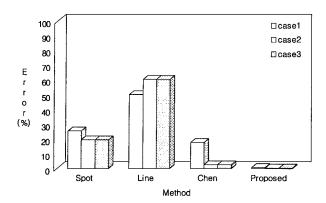


Fig. 5 An earthwork error of the terrain  $(20 + y)/\sqrt{x}$ 

times larger than that using a proposed method. Also, from the results of cases 1, 2, 3 of example 1 and 2 as shown in Table 7, 8, the error produced using an improper grid is  $2.3 \sim 9.4$  times larger than that using a proper grid.

## 4. Conclusions

In this paper a new formula has been developed for estimating the volume of a borrow pit excavaion based on an extension of the cubic spline polynomial without boundary condition. Because the grid of a borrow pit is constructed by choosing the variational points of the ground profile and dividing the area of the pit into rectangles of unequal interval, the presented formula can be applied to the case in which the pit is divided into a grid with unequal intervals. From this study, the following comments may be made:

- 1) The proposed method is applied to two examples and the results show that it is generally better than the spot height method, line of best fit method, Chen and Lin method.
- 2) we propose an algorithm of finding a spline surface which interpolates the given data and an appropriate method to calculate the earthwork. We present some computational results showing that our proposed method provides better accuracy than Chen and Lin's method.
- 3) For maximum accuracy in estimating the volume of a pit excvation, it is very important to select the proper points (the variational point of the ground profile) to construct the grid.

4) The mathematical models of the conventional methods have a common drawback, i.e., the modeling curves form peak points at the joints. To avoid this drawback, the cubic spline polynomial is chosen as the mathmatical model of the new method. From the characteristics of the cubic spline polynomial, the modeling curve of the new method is smooth and matches the ground profile well.

# Acknowledgement

This research was partially supported by Dongeui University (2002).

# References

Mun, D.Y., (1995). "A study on the earthwork calculation for reclamation", Int. J. of KCORE., Vol 9, No 1, pp 61-70.

Anderson, J.M., Michael, E.M. and Woolnough, D.E. (1985). Introduction to surveying, McGraw-Hill Book Co., Inc., New York.

Chambers, D.W. (1989). "Estimating pit excavation volume using unequal intervals", J. of ASCE, Vol 115, No 4, pp 390-411.

Chen, C.S. and Lin, H.C. (1991). "Estimating pit excavation volume using cubic spline volume formula, J. of ASCE, Vol 117, No 2, pp 51-66.

Easa, S.M. (1993). "Smooth boundary approximation for computing area of irregular region", J. of ASCE, Vol 119, No 3, pp 86-101.

Easa, S.M. (1988). "Estimating pit excavation volume using nonlinear ground profile", J. of ASCE, Vol 114, No 2, pp 71-83.

Farin, G. (1988). Curves and surfaces in computer aided geometric design. Academic Press Inc, New York.

Moffit. F.H. and Bossler, J.D. (1998). Surveying, Harper & Row Publishers Inc, New York.

2002년 5월 14일 원고 접수

2002년 7월 30일 최종 수정본 채택