## The Effect of Additives on Twinning in ZnO Varistors

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By comparison of the experimental results in two systems of ZnO varistors, it's appear that  $Sb_2O_3$  is the indispensable element for twinning in ZnO varistors and the  $Zn_7Sb_2O_{12}$  spinel acts as the nucleus to form twins.  $Al_2O_3$  is not the origin of twinning in ZnO varistor, but it was found that  $Al_2O_3$  could strengthen the twinning and form a deformation twinning by  $ZnAl_2O_4$  dragging and pinning effect. The inhibition ratios of grain growth and nonuniformity of two systems ZnO varistors increase with the increase of  $Al_2O_3$  content. The twins affect the inhibition of grain growth, the mechanism could be explained follow as: twins increase the mobility viscosity of ZnO grain and grain boundary, and drag ZnO grain and liquid grain boundary during the sintering, then the grain growth is inhibited and the microstructure becomes more uniform.

Key words: Twinning, ZnO Varistor, Al<sub>2</sub>O<sub>5</sub>, Sb<sub>2</sub>O<sub>5</sub>, Dragging and pinning effect, Deformation twinning, Nonuniformity

#### I. Introduction

Various additives are added into ZnO to improve physical properties of varistors.  $Bi_2O_3$  is used to form the grain boundary layer and  $Sb_2O_3$  is added to ZnO varistor to control densification and grain growth. The inhibition of grain growth by  $Sb_2O_3$  is considered to be dominated by a drag mechanism of  $Zn_7Sb_2O_{12}$  spinel and a reduction of grain boundary mobility due to twin formation in virtually all ZnO grain. Optimum addition of  $Al_2O_3$  to ZnO effectively improve the nonlinearity by delaying the onset of the upturn-voltage and inhabit the grain growth.  $^{3-6}$ 

Twinning is a common phenomena in ZnO varistors containing Sb<sub>2</sub>O<sub>3</sub>. 1,7-17) Wang. et al. 7) observed that grains in commercial ZnO varistors (Harris Co.) comprise twinning. Gupta<sup>8)</sup> noted that the grains in commercial polycrystalline ZnO varistors are always accompanied by twins. Senda and Bradt141 discussed the twinning mechanism in ZnO ceramics containing Sb<sub>2</sub>O<sub>3</sub>. In other hand, Kim and Goo<sup>13)</sup> researched the stacking layer of the cation and anion in the twin boundary of ZnO added with Sb<sub>2</sub>O<sub>3</sub>, Bi<sub>2</sub>O<sub>3</sub> and CoO in detail and identified that the cation and anion are associated closely with the twin boundary and described the head-to-head configuration which results from this twinning in the ZnO structure with polar hexagonal. However, there were no discussions about different additives on twinning in any literatures. Especially, there is no the research of effects of Al<sub>2</sub>O<sub>3</sub> on twinning. The purposes of this paper is to investigate complex effects of different additives on twinning and analyze the effect of twins on grain growth in ZnO varistors.

## **II. Samples Preparation**

ZnO varistor samples are prepared in two different systems to analyze the effects of Al<sub>2</sub>O<sub>3</sub> and Sb<sub>2</sub>O<sub>3</sub> on twinning. A-series consist of 7 compositions according to Al<sub>2</sub>O<sub>3</sub> contents in ZnO, 3wt%Bi<sub>2</sub>O<sub>3</sub>, 3.6wt%Sb<sub>2</sub>O<sub>3</sub>, 1.16wt%Co<sub>2</sub>O<sub>3</sub>, 0.88wt%NiO, 0.71wt%MnO<sub>2</sub>, 0.93wt%Cr<sub>2</sub>O<sub>3</sub> in Table 1. B-series are same with A-series beside Sb<sub>2</sub>O<sub>3</sub>.

ZnO varistor samples are made by the conventional technique.  $^{\scriptscriptstyle{(5)}}$  The mixtures of raw materials are dried by spraying at 8000 rpm and then pressed into discs at a pressure of 600 kg/cm². The pressed bodies are sintered at 1200°C for 2 hrs. in air and cooled to room temperature. The final size of samples is 15 mm in diameter and 1 mm in thickness. The samples are mechanially grounded by SiC papers and then polished with 1- $\mu$ m Al<sub>2</sub>O<sub>3</sub> powder. The

Table 1. The Compositions of ZnO Varistor Samples

| A-<br>Series | $ m ZnO$ -3.0wt%Bi2O3-3.6wt% $ m Sb_2O_3$ -16wt% $ m Co_2O_3$ -0.88wt% $ m NiO$ -0.71wt%MnO $_2$ -0.93wt% $ m Cr_2O_3$     | A1         | $\mathrm{Al_2O_3}$ -None    |
|--------------|----------------------------------------------------------------------------------------------------------------------------|------------|-----------------------------|
|              |                                                                                                                            | A2         | $Al_2O_3$ -0.005wt%         |
|              |                                                                                                                            | <b>A</b> 3 | $Al_2O_3$ -0.02wt%          |
|              |                                                                                                                            | A4         | $\mathrm{Al_2O_3}$ -0.1wt%  |
|              |                                                                                                                            | A5         | $\mathrm{Al_2O_3}$ -0.5 %   |
|              |                                                                                                                            | A6         | $\mathrm{Al_2O_3}$ -1.0wt%  |
|              |                                                                                                                            | A7         | $\mathrm{Al_2O_3}$ -5.0wt%  |
| B-<br>Series | $ m ZnO\text{-}3.0wt\%Bi_2O_3	ext{-} \ 1.16wt\%Co_2O_3	ext{-}0.88wt\% \ NiO\text{-}0.71wt\%MnO_2	ext{-}0.93wt\% \ Cr_2O_3$ | B1         | Al₂O₃ -None                 |
|              |                                                                                                                            | B2         | $Al_2O_3$ -0.005wt%         |
|              |                                                                                                                            | Вз         | $\mathrm{Al_2O_3}$ -0.02wt% |
|              |                                                                                                                            | B4         | $\mathrm{Al_2O_3}$ -0.1wt%  |
|              |                                                                                                                            | B5         | $\mathrm{Al_2O_3}$ -0.5wt%  |
|              |                                                                                                                            | B6         | $\mathrm{Al_2O_3}$ -1.0wt%  |
|              |                                                                                                                            | В7         | $\mathrm{Al_2O_3}$ -5.0wt%  |

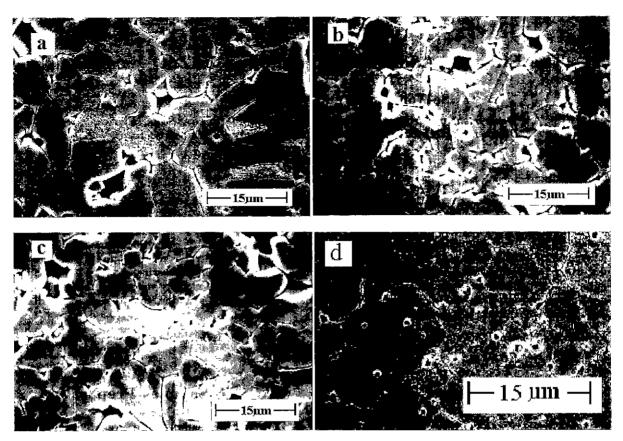


Fig. 1. SEM photos of twinning in commercial ZnO varistors with different  $Al_2O_3$  content, (a) 0 wt%, (b) 0.005 wt%, (c) 1wt%  $Al_2O_3$  and (d) sample of B series with 0.5 wt%  $Al_2O_3$ .

polished surfaces are etched with a 2% HClO<sub>s</sub>-ethanol solution and observed with a scanning electron microscope (SEM)(Hitachi, S-2700). X-ray diffraction analyser (Phillips, PW 1830) is used to analyse the crystalline phase of samples by using Al-K $\alpha$  target at 1.5°/min. scanning speed. Specimens for the transmisson electron microscope (TEM) (Hitachi, H-9000 NAR) are prepared by cutting 3 mm diameter disks with an ultrasonic cutter and grounded to less than 100  $\mu$ m with SiC papers and polished with 1  $\mu$ m Al<sub>2</sub>O<sub>3</sub> powder. The specimens are then thinned to 1000Å by ion milling method, and investigated at an acceleration voltage of 300 kV. The operating parameters of TEM are  $\lambda$ =1.8Å and camera length, L, of 50 cm.

### III. Results and Discussion

#### 1. The effect of Sb<sub>2</sub>O<sub>3</sub> on twinning in ZnO varistors

SEM photos of two different systems of ZnO varistors are given in Fig. 1. There are always twinning existing in ZnO grains of A-series, but no twnning in grains of Biseries. This phenomenon shows that the Al<sub>2</sub>O<sub>3</sub> dopant is not the origin of twinning in ZnO varistor.

Ordinally, commercial ZnO varistor consists of additions, such as Bi<sub>2</sub>O<sub>3</sub>, Co<sub>3</sub>O<sub>4</sub>, Cr<sub>2</sub>O<sub>3</sub>, MnO<sub>2</sub>, Sb<sub>2</sub>O<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub> and Nb<sub>2</sub>O<sub>5</sub>. Gupta<sup>5)</sup> reported that ZnO varistor containing Bi<sub>2</sub>O<sub>5</sub> and other additions, such as Co, Mn, and Sb etc., generated

crystallographic twins. But there was not twinning existing in ZnO-Pr<sub>6</sub>O<sub>11</sub> varistors containing Co, K, Cr, etc. additions. 9,11) Senda and Bradt17 and Gupta8 did not observe twinning in pure ZnO and ZnO-Bi<sub>2</sub>O<sub>3</sub> varistor, but twinning was always observed in ZnO varistors with Sb<sub>2</sub>O<sub>3.10</sub> From our observation in two different systems of ZnO varistors and results in other literatures mentioned above, it is evident that Sb<sub>2</sub>O<sub>3</sub> act as the indispensable element for twinning in ZnO varistors. Senda and Bradt<sup>1</sup> analyzed the formation intensity of the twinning to Sb<sub>2</sub>O<sub>3</sub> added to pure ZnO. They observed a single twin boundary in every ZnO, regardless of the Sb<sub>2</sub>O<sub>3</sub> content, the sintering temperature or the grain size of the ZnO ceramics. It was statistically studyed by Yamamoto  $et\ al.^{9,11)}$  that the individual twin boundary was always located at or near to the center of the ZnO grain. Similarly, in our experimental results, it was observed that all twins are single ones located at or near to the centers of ZnO grains from the SEM photo of sample A1 without Al<sub>2</sub>O<sub>3</sub> in Fig. 1(a).

Fig. 2(a), (b) are the TEM photos of selected-areadiffraction pattern (SADP) and the bright-image in the ZnO grain of sample A4, respectively. The bright-image in Fig. 2(b) shows a continuous thickness fringes across the ZnO grain, which are known as a typical phnomenon of twinning.<sup>14)</sup> Then, the selected-area-diffraction pattern (SADP) at the [1-1 1] zone axis is illustrated in Fig. 2(a).

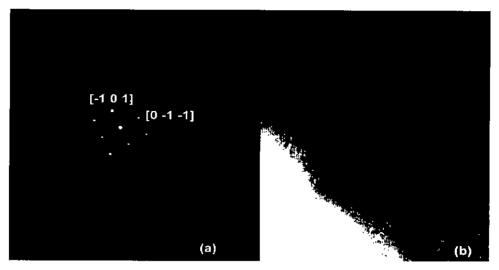


Fig. 2. TEM photos of twins in the ZnO grain of sample A4  $(0.1\text{wt\% Al}_2\text{O}_3\text{ content})$  (a) the selected-area-diffraction pattern (SADP) and (b) the bright-image.

ZnO has the wurtzite structure and belongs to th P6amc space group which is hexagonal and polar. The wurtzite suructure of ZnO can be described as a close packed oxygen anion structure consisting of layer of oxygen anions with the smaller zinc cations located at the tetrahedral interstics. It is nesssary to consider if either the antimony oxide or the Zn<sub>2</sub>Sb<sub>2</sub>O<sub>12</sub> spinel structure may have any relationship or potential effect on the ZnO structure to twin. The spinel structure is not too different in its atomic arrangement from the wurtzite structure, as it also consists of stacked layers of colse packed oxygen anions. 13,12) This suggests that perhaps the twinning condition that is created by the addition of antimony oxide to ZnO may be similar in its fundamental nature to the traditional hexagonal/cubic/hexagonal stacking layer sequency wihich so often occurs for the twinning of hexagonal meterials.12)

# 2. Strengthening effect of $Al_2O_3$ on twinning and deformation

The number of twins and ZnO grains number were counted from the SEM photo and the ratio of twinning was calculated with  $Al_2O_3$  contents, which is illustrated in Fig. 3. As discussed above, the  $Al_2O_3$  dopant is not the origin of twinning in ZnO varistor, but the twinning ratio increases obviously with the increase of  $Al_2O_3$  content. When  $Al_2O_3$  content reaches 1wt%, about 50-60 percent of ZnO grains was twins. Therefore, it appears that the  $Al_2O_3$  is not the origin of twinning in ZnO varistors, but it promotes twin formation.

The microstructures of twins with Al<sub>2</sub>O<sub>3</sub> are not same with those in ZnO-Sb<sub>2</sub>O<sub>3</sub> and ZnO-Sb<sub>2</sub>O<sub>5</sub>-Bi<sub>2</sub>O<sub>3</sub> systems varistors. Only a part of twins with Al<sub>2</sub>O<sub>3</sub> have twin grain boundary always located at or near to the center of the ZnO grain caused by grain growth mechanism. <sup>14</sup> And other twin boundaries show a complicated shapes. When

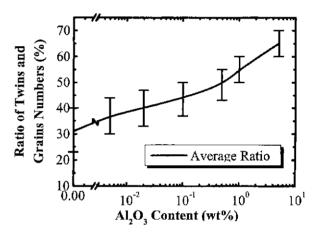


Fig. 3. The ratio of twinning with different Al<sub>2</sub>O<sub>3</sub> contents.

the Al<sub>2</sub>O<sub>3</sub> content is small, a large number of twins are growth twins and complicated twins are observed only few. But the portion of grains having complicated twin boundaries increase with the increase of Al<sub>2</sub>O<sub>3</sub> content. The typical SEM photo of complicated twins are shown in Fig. 4. We can observe No.2, No.3, No.6, No.8, No.12, No.17, No.18 grains have growth twins; No.1 and No.13 grains have zigzag twin boundaries; No. 7 and No.14 grains have "Z" shape twin boundaries; No.10, No.11, and No.16 have triangle twin boundaries. In the results, it would be said that these complicated twins are belong to a kind of deformation twins.<sup>141</sup>

The possible mechanism to generate deformation twinning could be explained when  $Al_2O_3$  is added to  $ZnO-Bi_2O_3$ - $Sb_2O_3$  system ZnO varistors. During sintering,  $Al_2O_3$  reacts with ZnO to form  $ZnAl_2O_4$  spinel, which was observed by X-ray diffraction of ZnO varistors as given in Fig. 5. But the  $ZnAl_2O_4$  spinel can not act as nucleus to form twin like  $Zn_7Sb_2O_{12}$  spinel, because twinning is not

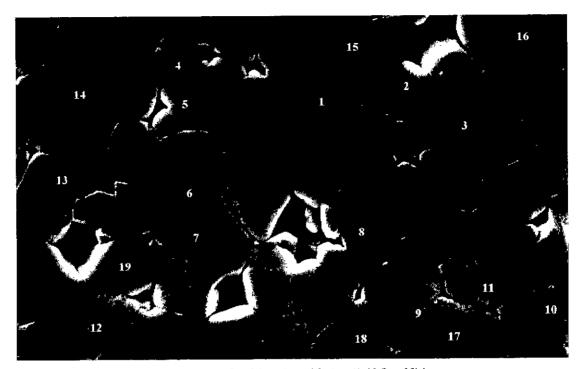


Fig. 4. The deformation twins in ZnO varistor sample of A-series with 1 wt% Al<sub>2</sub>O<sub>3</sub> addition.

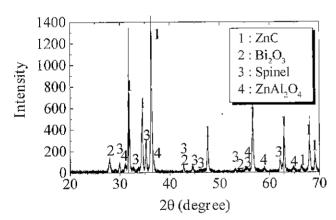


Fig. 5. X-ray diffraction pattern of commercial ZnO varistor with 5 wt% Al<sub>2</sub>O<sub>3</sub>.

observed in ZnO-Bi $_2$ O $_3$ -Al $_2$ O $_3$  system ceramics. As discussed by other researchers, <sup>3,6)</sup> ZnAl $_2$ O $_4$  spinel inhibit the grain growth by dragging and pinning effect at the grain boundary. Then mechanical stress would be generated when ZnO grain collide with ZnAl $_2$ O $_4$  spinel due to thermal motion. In the other hand, thermal stresses would be developed between the ZnO primary and the ZnAl $_2$ O $_4$  spinel as a sequence of thermal expansion due to the mismatch of those phases. The mechanical and thermal stresses would lead to deformation twinning. Where it was known that the small thermal stress could not generate the serious deformation twin in ZnO varistors. <sup>16</sup>

Consequently, when the ZnAl<sub>2</sub>O<sub>4</sub> spinel pins in the grain boundary during sintering, it blocks the motion of

liquid  $\mathrm{Bi_2O_3}$  grain boundary by dragging and pinning effect and then its wrapping effect to  $\mathrm{Zn_7Sb_2O_{12}}$  spinel would be reduced, and more twins are generated. With the increase of  $\mathrm{Al_2O_3}$  content, more  $\mathrm{ZnAl_2O_4}$  spinels would be formed and then the blocking effect to liquid  $\mathrm{Bi_2O_3}$  grain boundary increases. This causes the wrapping effect weaken and then more  $\mathrm{Zn_7Sb_2O_{12}}$  spinels are free to form twins as nuclei. In the other hand, the mechanical stress generated by ZnO grain colliding with  $\mathrm{ZnAl_2O_4}$  spinel due to thermal motion increases, and leads to form more deformation twins.

## 3. Inhibiton effect of twins on grain growth in ZnO varistors

To estimate the inhibition effects on grain growth in ZnO varisors, the average intercept length and its respective standard deviation of ZnO varistor grains are used. The inhibition of grain growth is observed with the increase of Al<sub>2</sub>O<sub>3</sub> contents in two systems as discussed in literature.<sup>2,3)</sup> The standard deviation becomes smaller, and the microstructure of ZnO varistor becomes more uniform with the increase of Al<sub>2</sub>O<sub>3</sub>.

In order to analyze the effect of  $\mathrm{Al_2O_3}$  on grain growth, the inhibition ratio of grain growth and nonuniformity inhibition ratio are calculated. Then, the inhibition ratio of grain growth  $\mathrm{K_g}$  is defined as

$$K_g = (D_0 - D_t)/D_0,$$
 (1)

here,  $D_0$  is the average grain size of the sample of Bseries without  $Al_2O_3$ , and  $D_i$  is the average grain size of sample of A and B-series with i wt%  $Al_2O_3$ . And the

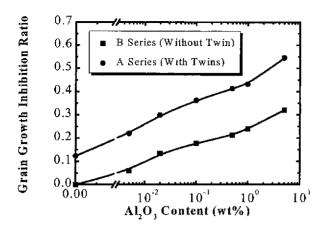


Fig. 6. The inhibition ratio of Grain growth with different Al<sub>2</sub>O<sub>3</sub> contents.

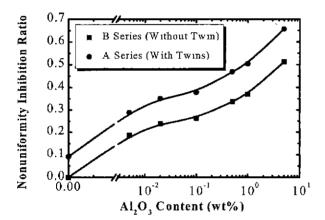


Fig. 7. Nonuniformity inhibition ratio of with different  $Al_2O_3$  contents.

nonuniformity inhibition ratio K<sub>u</sub> is defined as

$$K_{u} = (\sigma_{0} - \sigma_{i})/\sigma_{0}, \qquad (2)$$

here,  $\sigma_0$  is the standard deviation of the sample of B-series without  $Al_2O_3$  and  $\sigma_\epsilon$  is the standard deviation of sample in A and B-series with  $\iota$  wt%  $Al_2O_3$ . Because the grain growth of the sample of B-series without  $Al_2O_3$  is not affected by  $Al_2O_3$ ,  $Sb_2O_3$  and twin, its average and standard deviation are used as the comparing criterion to calculate  $K_c$  and  $K_u$ . Therefore, higher  $K_z$  is, better the inhibition effect is and higher  $K_u$  is, more uniform the ZnO varistor is.

Fig. 6 and Fig. 7 show that the inhibition ratios of grain growth and nonuniformity of two systems ZnO varistors increase with the increase of Al<sub>2</sub>O<sub>3</sub> content. As discussed by Nunes and Bradt, Quadir and Readey, Al<sub>2</sub>O<sub>3</sub> reacts with ZnO to form ZnAl<sub>2</sub>O<sub>4</sub> spinel during sintering. ZnAl<sub>2</sub>O<sub>4</sub> spinel inhabits the grain growth by dragging and pinning effects. So, because more ZnAl<sub>2</sub>O<sub>4</sub> spinels are formed, the inhibition effect on grain growth is stronger and the the microstructure of ZnO varistor becomes more uniform with the increase of Al<sub>2</sub>O<sub>3</sub> content.

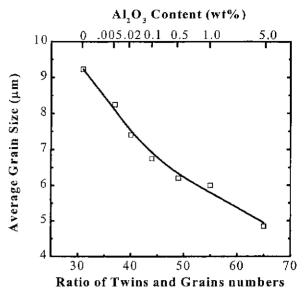


Fig. 8. The relation between the average grain size and the ratio of twins and grains numbers of ZnO varistors.

In other hand, when Sb<sub>2</sub>O<sub>J</sub> is added into ZnO varistor, the Zn<sub>7</sub>Sb<sub>2</sub>O<sub>12</sub> spinel inhibits the grain growth, too. Senda and Bradt<sup>11</sup> suggested that Sb<sub>2</sub>O<sub>3</sub> effect on grain growth inhibition in ZnO-Sb<sub>2</sub>O<sub>3</sub> system varistor. They supposed that both the Zn<sub>7</sub>Sb<sub>2</sub>O<sub>12</sub> spinel and the twins are responsible for the ZnO grain growth inhibition by Sb<sub>2</sub>O<sub>3</sub>.

All samples in B-series do not contain any twin. So the inhibition of grain growth in B-series is the only effect of  $Al_2O_3$ . But in A-series with  $Sb_2O_3$ , all samples have twins. As a result, the inhibition ratio of grain growth in A-series is the total effect by  $Al_2O_3$ ,  $Sb_2O_3$  and twins.

The relationship among twins ratio,  $Al_2O_3$  content and average grain size of A-series ZnO varistors are given in Fig. 8. When  $Al_2O_3$  is added into A-series ZnO varistors, the twin obviously increases with the increase of  $Al_2O_3$  content. This result appears that  $Al_2O_3$  affects the twin formation,

If the twins do not affect the ZnO grain growth and the uniformity in ZnO varistors, then there should be only a constant differences between two curves in Fig. 6 and Fig. 7 for simplification, where, the constant differences is the influence of  $\mathrm{Sb_2O_3}$  on grain growth inhibition by the dragging effect of formed  $\mathrm{Zn_7Sb_2O_{12}}$  spinel. But according to our experimental results, it is shown that there are the difference existing in two different systems ZnO varistors and the difference becomes larger with the increase of  $\mathrm{Al_2O_3}$  content.

The effects of only twins on ZnO grain growths and the uniformity in microstructures of ZnO varistors are given in Fig. 9 and Fig. 10. However, the differences contain the effects of the  $\rm Zn_7Sb_2O_{12}$  spinel, which are difficult to be expelled from those differences. The inhibition ratios of grain growth and the nonuniformity increases obviously with the increase of twins in Fig. 9

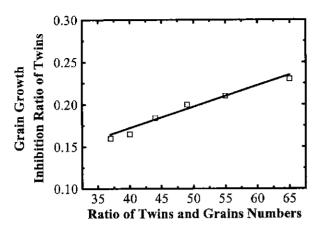


Fig. 9. Twins effect on the inhibition of ZnO grain growth in ZnO varistors.

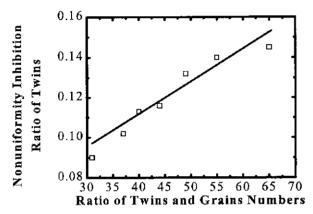


Fig. 10. Twins effect on the nonuniformity in microstructure of ZnO varistors.

and Fig. 10. Therefore, it is comfirmed that the twins have identically effects on the ZnO grain growths and the uniformity in microstructures of ZnO varistors.

#### IV. Conclusions

- 1. By comparison of the experimental results in two different systems of ZnO varistors, it is shown that  $\mathrm{Sb_2O_3}$  acts as the indispensable element for twinning in ZnO varistors and the  $\mathrm{Zn_7Sb_2O_{12}}$  spinel acts as nuclei to form twins.
- 2. The Al<sub>2</sub>O<sub>3</sub> dopant is not the origin of twinning in ZnO varistor, but Al<sub>2</sub>O<sub>3</sub> promoted the twinning and formed ZnAl<sub>2</sub>O<sub>4</sub> which deformed twinning by dragging and pinning.
- 3. The inhibition ratios of grain growth and nonuniformity of two systems ZnO varistors increase with  ${\rm Al_2O_3}$  content.
- 4. The twins affects the inhibition of ZnO grain growth. Grain inhibition mechanism by twins could be explained that the twins decrease the mobility of ZnO grain and

increase of viscosity of grain boundary, and drag ZnO grain and liquid grain boundary, and then the grain growth is inhibited and the microstructure becomes more uniform.

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