

## Reaction Synthesis and Mechanical Properties of $B_4C$ -based Ceramic Composites

Jae-Ho Han <sup>1,a</sup>, Sang-Whan Park <sup>2,b</sup> and Young-Do Kim <sup>1,c</sup>

<sup>1</sup>Division of Materials Science & Engineering, Hanyang Univ., Seoul 133-791, Korea

<sup>2</sup>Multifunctional Ceramics Research Center, KIST, Seoul, Korea

<sup>a</sup>jh\_han@kist.re.kr, <sup>b</sup>spark@kist.re.kr, <sup>c</sup>ydkim1@hanyang.ac.kr

### Abstract

In this investigation,  $B_4C$  based ceramic composites were fabricated by in-situ reaction hot pressing using  $B_4C$ , TiC and SiC powder as starting materials. The reaction synthesized composites by hot pressing at 1950 °C was found to possess very high relative density. The reaction synthesized  $B_4C$  composites comprise  $B_4C$ ,  $TiB_2$ , SiC and graphite by the reaction between TiC and  $B_4C$ . The newly formed  $TiB_2$  and graphite was embedded both inside grain and at grain boundary of  $B_4C$ . The mechanical properties of reaction synthesized  $B_4C$ - $TiB_2$ -SiC-graphite composites were more enhanced compared to those of monolithic  $B_4C$ .

**Keywords :**  $B_4C$ , composite, reaction synthesis, mechanical property

### 1. Introduction

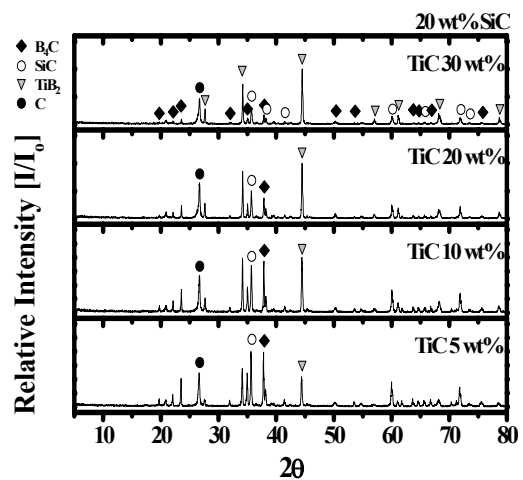
$B_4C$  based ceramics exhibits many attractive properties for structural materials such as high melting point, low density, good chemical stability, high wear resistance, and high hardness, which enables them to be used for wear resistant parts, light weight armor, and cutting tool [1-4]. However,  $B_4C$ -based ceramics have some major problems such as low strength and fracture toughness compared with other competitive engineering ceramics such as  $Si_3N_4$  and SiC. Furthermore,  $B_4C$ -based ceramics have very poor sinterability due to its low self diffusion coefficient. Many researches have been performed to improve the mechanical properties as well as sinterability of  $B_4C$ -based ceramics [3-12]. The studies reveal that it would be a challenge to achieve both improvements in sinterability and mechanical properties. Therefore, in this study, reactive sintering process was performed to prepare fully dense  $B_4C$ -based ceramic composites by adding SiC and TiC into  $B_4C$  matrix at a relatively low temperature. The effect of adding SiC and TiC on sinterability and mechanical properties of  $B_4C$ -based ceramic composites was investigated.

### 2. Experimental and Results

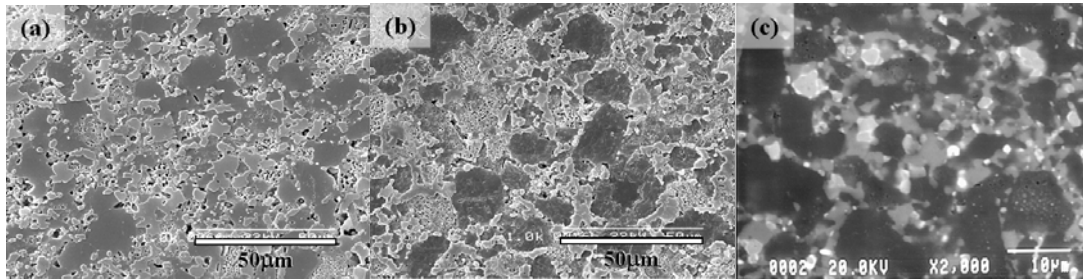
In this study,  $B_4C$ , TiC, and SiC powder were used as starting materials.  $B_4C$ , SiC, and TiC powder were mixed with a composition of  $B_4C : SiC : TiC = 50\sim75 : 20 : 5\sim30$  in wt. % using SPEX™ mill for 10 min in Ar atmosphere.  $B_4C$ -based ceramic composites were fabricated by hot pressing at the temperature range of 1950 °C under 40 MPa for 0.5 h in Ar atmosphere. After the fabrication process, phase identifications of fabricated  $B_4C$ -based

ceramic composites were done by X-ray diffraction (XRD) method with Cu-k radiation. The polished surface of fabricated  $B_4C$ -based ceramic composites was electrochemically etched in 20%  $HNO_3$  solution, and then examined by scanning electron microscope (SEM). The three-point bending tests were performed to measure the toughness by single edge notched beam method of  $B_4C$ -based ceramic composites specimen with dimensions of about 3 x 4 x 25 mm.

Fig.1 shows XRD patterns of fabricated  $B_4C$ -based ceramic composites by hot pressing. The crystalline phases in  $B_4C$ -based ceramic composites comprise  $B_4C$ ,  $TiB_2$ , SiC, and graphite. With increasing TiC content in starting

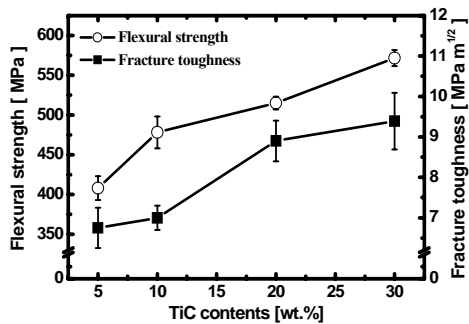


**Fig. 1.** XRD patterns of  $B_4C$  composites fabricated by hot pressing at 1950 °C.



**Fig. 2.** SEM microstructures of B<sub>4</sub>C composites by hot pressing of (a) 75 w/o B<sub>4</sub>C:20 w/o SiC:5 w/o TiC, (b) 70 w/o B<sub>4</sub>C: 20 w/o SiC: 10 w/o TiC, and (c) back scattered SEM microstructure of (b).

materials, intensities of XRD peaks for TiB<sub>2</sub> and graphite increases as shown in Fig. 1. Fig. 2 shows the SEM microstructures of fabricated B<sub>4</sub>C-based ceramic composites. SiC and newly formed phases were relatively well distributed inside B<sub>4</sub>C grain as well as along the B<sub>4</sub>C grain boundaries. With increase TiC content, newly formed phases and SiC dispersions formed another interconnected matrix along with B<sub>4</sub>C matrix. From the EDS analysis, dispersions as shown in Fig. 3(c), the gray colored and white colored phase were identified as SiC and newly formed TiB<sub>2</sub> phase, respectively. Fig. 3 shows the flexural strength and fracture toughness of B<sub>4</sub>C-based ceramic composites fabricated in this study.



**Fig. 3.** Flexural strength and fracture toughness of B<sub>4</sub>C composites fabricated by hot pressing.

Both flexural strength and fracture toughness of B<sub>4</sub>C-based ceramic composites almost linearly increase with the content of TiC in the starting material. For the B<sub>4</sub>C-based ceramic composites with TiC content of 30 wt.%, flexural strength and fracture toughness were about 570 MPa and 9.5 MPa<sup>1/2</sup>, respectively.

### 3. Summary

In this study, B<sub>4</sub>C-TiB<sub>2</sub>-SiC-graphite composites were synthesized by reactive hot pressing using B<sub>4</sub>C, TiC and SiC powder as starting materials. The mechanical properties of reaction synthesized B<sub>4</sub>C-TiB<sub>2</sub>-SiC-graphite composites fabricated in this study showed significant improvements compared to those of monolithic B<sub>4</sub>C and other B<sub>4</sub>C-based ceramic composites reported in the previous studies. The flexural strength and fracture toughness of these in-situ B<sub>4</sub>C synthesized composites were 400-570 MPa and 6-9.5 MPa<sup>1/2</sup>, respectively. The enhanced fracture toughness of B<sub>4</sub>C based ceramic composites are considered to be due to the severe crack deflection at the phase boundary between B<sub>4</sub>C matrix and dispersions consisting of SiC and TiB<sub>2</sub>, which occur by residual stress from the difference in thermal expansion coefficients of B<sub>4</sub>C, SiC, and TiB<sub>2</sub> upon cooling from the fabrication temperature.

### 4. References

1. H. Nishikawa: Ceramics Vol. 22 (1987), p. 40
2. W. C. Johnson.: Am. Ceram. Soc. Bull. Vol. 80 (2001), p. 64
3. F. Thevenot: J. Eur. Ceram. Soc. Bull. Vol. 6 (1990), p. 205
4. F. Thevenot: Key Eng. Mat. Vol. 56-57 (1991), p. 59
5. K. Schwetz, et al.: J. Solid State Chem. Vol. 133 (1997), p. 68
6. L. S. Sigl: J. Eur. Ceram. Soc. Vol. 18 (1998), p. 1521
7. D. K. Kim and C. H. Kim: Adv. Ceram. Mater. Vol. 3 (1988), p. 52
8. G. J. Zhang, et al.: Mater. Lett. Vol.25 (1995) p. 97
9. S. Yamada, et al.: J. Eur. Ceram. Soc. Vol. 23 (2003) p. 561
10. Z. Yuhua, et al.: Mater. Res. Bull. Vol 39 (2004), p. 1615
11. S. Li, et al.: Mater. Lett. Vol. 57 (2003), p. 1445-1452(2003)
12. S. Li: Mater. Sci. & Eng. A Vol. 332 (2002), p. 37