

## Mechanical Properties and Microstructure of Aluminum Alloys with Dispersed Nanoscale Quasicrystalline Particles

Masashi Fujita<sup>1,a</sup>, Hisamichi Kimura<sup>2,b</sup>, and Akihisa Inoue<sup>3,c</sup>

<sup>1</sup>Honda R&D Co., Ltd 4630 Shimotakanezawa, Haga-machi, Haga-gun, Tochigi, 321-3393 Japan

<sup>2,3</sup>Institute of Material Research, Tohoku university, Sendai 980-8577, Japan

<sup>a</sup>masashi\_fujita@n.t.rd.honda.co.jp, <sup>b</sup>hisami@imr.tohoku.ac.jp, <sup>c</sup>ainoue@imr.tohoku.ac.jp

### Abstract

*New Al-based alloys with very high ultimate tensile strength were developed in high Al concentration range of 91-95 at.% for Al-Fe-Cr-Ti-M (M: Co and Mo) systems and Al-Fe-Cr-Mo-Ti-Co system by the dispersion of nanoscale quasicrystalline particles in Al phase. The effect of adding elements, M was discussed in the viewpoint of stability of super-cooled liquid state and formation ability of quasicrystalline phase. The P/M Al-Fe-Cr-Ti-M alloys with dispersed nanoscale quasicrystalline particles exhibited ultimate tensile strength of 350MPa at 573K and 200MPa at 673K.*

**Keywords:** aluminum-based alloy, quasicrystalline phase, powder metallurgy, high elevated-temperature strength

### 1. Introduction

It is known that quasicrystalline (Q.C.) alloys with stoichiometric compositions have high Vickers hardness ( $H_v$ ) and extremely brittle nature. For example,  $H_v$  is 1010 for the rapidly solidified (RS) Q.C.  $Al_{77.5}Mn_{22.5}$  alloy<sup>1)</sup>, 710 for the RS Q.C.  $Al_{85.6}Cr_{15.4}$  alloy<sup>1)</sup> and 735 for the RS Q.C.  $Al_{86}V_{14}$  alloy<sup>2)</sup>. These alloys also have high thermal stability. The volume fraction of the Q.C. particles decreases in order of  $Cr > Mn > V$  in the powder metallurgy (P/M)  $Al_{93}Fe_3M_2Ti_2$  (M: V, Cr, Mn) alloys<sup>3)</sup>. There is a possibility of synthesizing a new material with high specific strength, high elevated-temperature strength and high wear resistance by dispersing Q.C. particles into fcc-Al phase. The P/M  $Al_{94}V_4Fe_2$  and  $Al_{93}Fe_3Cr_2Ti_2$  alloys containing quasicrystalline phase have high strength exceeding 580MPa<sup>4)</sup>, high-elevated temperature strength exceeding 300MPa at 573K, and much better wear resistance than commercial A390 aluminum alloy<sup>4)</sup>. This paper presents the microstructure and mechanical properties for Al-Fe-Cr-Ti-M (M: Co and Mo) alloys and Al-Fe-Cr-Mo-Ti-Co alloy produced by melt spinning technique and powder metallurgy technique.

### 2. Experimental procedures

The alloy ingots were prepared by arc melting pure metals where their purity is better than 99.85% in an argon atmosphere. From the ingots, RS alloys with a cross section of  $0.02 \times 1 \text{ mm}^2$  were produced by a melt spinning technique. The ingots of powder metallurgy (P/M) alloys were prepared by induction melting in an argon atmosphere.

Rapid solidified (RS) powders were produced by high pressure gas and water atomization process<sup>5)</sup>, followed by sieving into the sizes smaller than 150  $\mu\text{m}$ . By using the conventional powder metallurgy technique, P/M Al-Fe-Cr-Ti-M alloys with a diameter of 10 mm and a length of 600 mm were produced by extrusion of the atomization powders. The structure of RS and P/M alloys were examined by X-ray diffraction and transmission electron microscopy (TEM). Tensile strength was measured at a strain rate of  $4.0 \times 10^{-4} \text{ s}^{-1}$  in the temperature range from room temperature to 673 K with an Instron testing machine.

### 3. Results and Discussion

3-1. Microstructure of RS  $(Al_{0.93}Fe_{0.03}Cr_{0.02}Ti_{0.02})_{100-x}M_x$  (M: Co and Mo,  $x=0, 2$  and  $3$ ) alloy ribbons

Figure 1 shows X-ray diffraction patterns of the RS  $(Al_{0.93}Fe_{0.03}Cr_{0.02}Ti_{0.02})_{100-x}Co_x$  ( $x=0, 2$  and  $3$ ) alloy ribbons produced by a melt spinning technique at the copper roller circumferential velocity ( $V_c$ ) of 40m/s. The X-ray diffraction peaks broaden by adding cobalt element compared with  $Al_{93}Fe_3Cr_2Ti_2$  alloy. The X-ray diffraction pattern shows an amorphous single phase when Co is added to 3at%. This means that addition of cobalt stabilizes the super-cooled liquid state of Al-Fe-Cr-Ti alloy.

Figure 2 shows X-ray diffraction patterns of the RS  $(Al_{0.93}Fe_{0.03}Cr_{0.02}Ti_{0.02})_{98}M_2$  (M=None, Mo) alloy ribbons produced by a melt spinning technique at the copper roller of  $V_c=20\text{m/s}$ . The X-ray diffraction peaks of the  $Al_{93}Fe_3Cr_2Ti_2$  alloy consist of fcc-Al, quasicrystalline (Q.C.) and  $Al_{23}Ti_9$  phases. On the other hand, by addition of 2 at% Mo, the intermetallic compound peaks disappear and the quasicrystalline peaks become very clear. This

means that molybdenum imparts a better formation ability of quasicrystalline phase to Al-Fe-Cr-Ti alloy.

In alloy design to disperse nanoscale Q.C. particles into fcc-Al phase, it is definitely important to consider the balance between the stability of super-cooled liquid state and the formation ability of quasicrystalline phase. In this study, Co and Mo are added to Al-Fe-Cr-Ti alloy to balance those two issues.

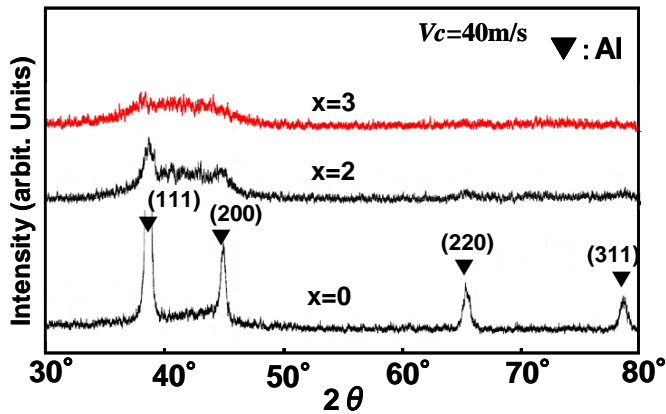


Fig. 1. X-ray diffraction patterns of the RS ( $\text{Al}_{0.93}\text{Fe}_{0.03}\text{Cr}_{0.02}\text{Ti}_{0.02}$ ) $_{100-x}\text{Co}_x$  alloys.

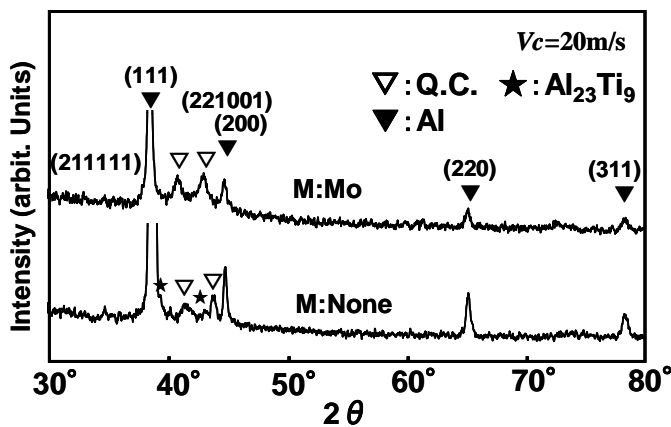


Fig. 2. X-ray diffraction patterns of the RS ( $\text{Al}_{0.93}\text{Fe}_{0.03}\text{Cr}_{0.02}\text{Ti}_{0.02}$ ) $_{98}\text{M}_2$  alloys

### 3-2. Microstructure and mechanical properties of P/M $\text{Al}_{93}\text{Fe}_{2.45}\text{Cr}_{2.45}\text{Mo}_{0.5}\text{Ti}_{0.8}\text{Co}_{0.8}$ alloy

Figure 3 shows the temperature dependence of the ultimate tensile strength ( $\sigma_{\text{UTS}}$ ) for the P/M  $\text{Al}_{93}\text{Fe}_{2.45}\text{Cr}_{2.45}\text{Mo}_{0.5}\text{Ti}_{0.8}\text{Co}_{0.8}$  alloy at each testing temperature, together with the data of  $\text{Al}_{93}\text{Fe}_3\text{Cr}_2\text{Ti}_2$  alloy and the conventional Al-based alloy. The  $\sigma_{\text{UTS}}$  show much higher ones over the whole temperature range up to 673 K as compared with those of conventional Al alloys with high elevated-temperature strength.

Figure 4 shows bright field electron micrograph and selected-area electron diffraction pattern of the P/M  $\text{Al}_{93}\text{Fe}_{2.45}\text{Cr}_{2.45}\text{Mo}_{0.5}\text{Ti}_{0.8}\text{Co}_{0.8}$  alloy. One can see the

spherical Q.C. particles with a grain size of about 100 nm dispersed uniformly into fcc-Al matrix.

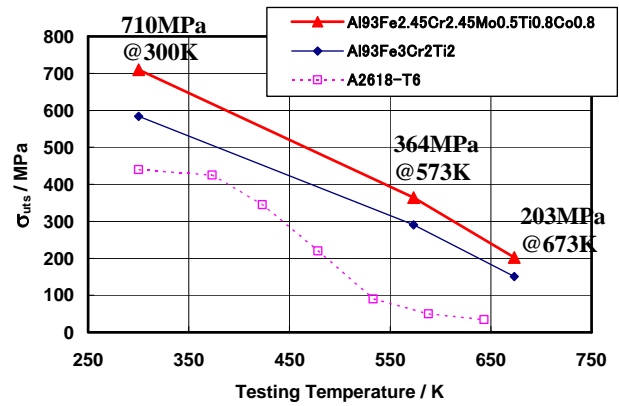


Fig. 3. Temperature dependence of ultimate tensile strength ( $\sigma_{\text{UTS}}$ ) as a function of testing temperature for the P/M  $\text{Al}_{93}\text{Fe}_{2.45}\text{Cr}_{2.45}\text{Mo}_{0.5}\text{Ti}_{0.8}\text{Co}_{0.8}$  alloy.

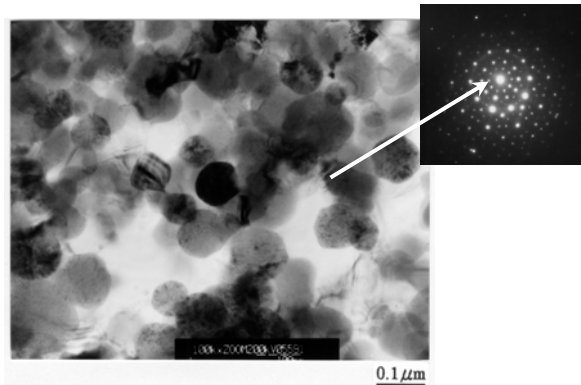


Fig. 4. Bright field electron micrograph and selected-area diffraction pattern of the P/M  $\text{Al}_{93}\text{Fe}_{2.45}\text{Cr}_{2.45}\text{Mo}_{0.5}\text{Ti}_{0.8}\text{Co}_{0.8}$  alloy.

### 3. Summary

By addition of Co and Mo to Al-Fe-Cr-Ti alloy the good balance between the stability of super-cooled liquid state and the formation ability of quasicrystalline phase was obtained. The P/M Al-Fe-Cr-Ti-Co-Mo alloy with dispersed nanoscale quasicrystalline particles exhibited ultimate tensile strength of more than 350 MPa at 573 K and 200 MPa at 673 K.

### 4. References

1. A. Inoue, J. Mater. Sci., 22 (1987), 1758.
2. H. M. Kimura, J. Jpn. Inst. Light Met., 48 (1988), 127.
3. H. M. Kimura, J. Jpn. Soc. Powder Met., 46 (1999), 1321.
4. H. M. Kimura, Mater. Trans. JIM, 41 (2000), 1550.
5. K. Ichikawa, Metals, 65 (1995), 1165.