

Fig. 3. The Miller capacitance.

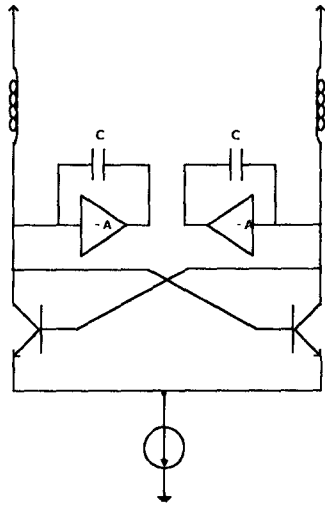


Fig. 4. Conventional BJT VCO using negative feedback Miller capacitance

In this paper is newly proposed VCO using miller effect. This main idea is to control effective capacitance lower and upper than reference frequency, which can be realized using the positive and negative feedback of Miller effect capacitance.

2.1. Negative Feedback Miller Capacitance

Fig. 5 shows the LC-oscillator using negative feedback Miller capacitance. This VCO oscillates at lower frequencies than the reference frequency by variable gain amplifier. The effective capacitance value is $C(1-(-A))$. So the oscillation frequency is lower than the reference frequency.

2.2. Positive Feedback Miller Capacitance

Fig. 6 shows the LC-oscillator using positive feedback Miller capacitance. This differential oscillator makes a 180 degree phase difference between node A and node B in Fig. 6. The oscillation signal from node A (V_a) amplified by the negative gain becomes $-A \cdot V_a = A \cdot V_b$. Therefore the effective Miller capacitance is $C(1-A)$ ($A > 0$). The 180 degree phase difference between node A and node B and the negative amplifier gain gives the positive feedback Miller effect. So the effective Miller capacitance $C(1-A)$ ($A > 0$) is lower than the feedback capacitance C and the oscillation frequency is higher than the reference frequency.

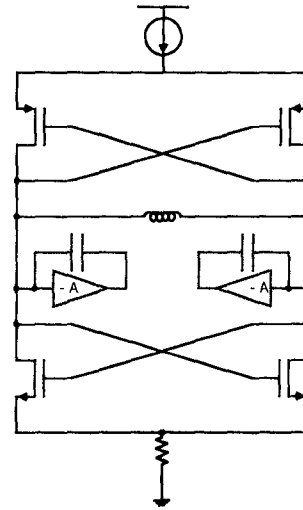


Fig. 5. LC-oscillator using negative feedback Miller capacitance.

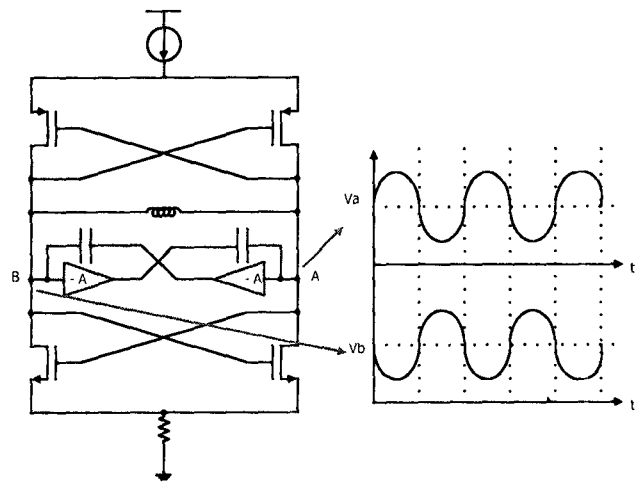


Fig. 6. LC-oscillator using positive feedback Miller capacitance.

3. PROPOSED VCO AND SIMULATION RESULTS

Fig. 7 shows the positive and negative feedback control circuit. This is basically cascode structure. Ma_2 and Ma_3 is switched by the control signal V_a and V_b . Fig. 8 shows complete proposed VCO schematic. In Fig. 8, the negative feedback loop consists of Ma_1 , Ma_3 and capacitance C_{fn} and the positive feedback loop consists of Ma_1 , Ma_2 and capacitance C_{fp} . The proposed VCO is simulated using HSPICE based on 0.25um standard CMOS technology. As can be seen in Fig. 9, the negative feedback mode frequency tuning range is 400 MHz, from 2.86 GHz to 2.45 GHz and positive feedback mode frequency tuning range is 220 MHz, from 2.86 GHz to 3.08 GHz. The simulated frequency tuning range is about 23% of the central frequency. The calculated phase noise using simple model [7] is -104dBc/Hz at 1MHz offset. The operating current is 3.84 mA (max.) and 2.14 mA (min.) at 2.5V power supply. The summary of the simulation results of the proposed LC-oscillator is described in Table 1.

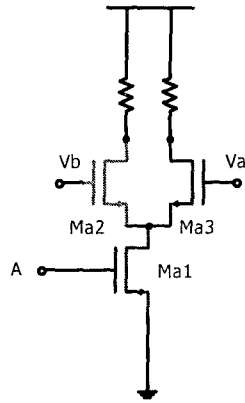


Fig. 7. Control circuit of negative and positive feedback.

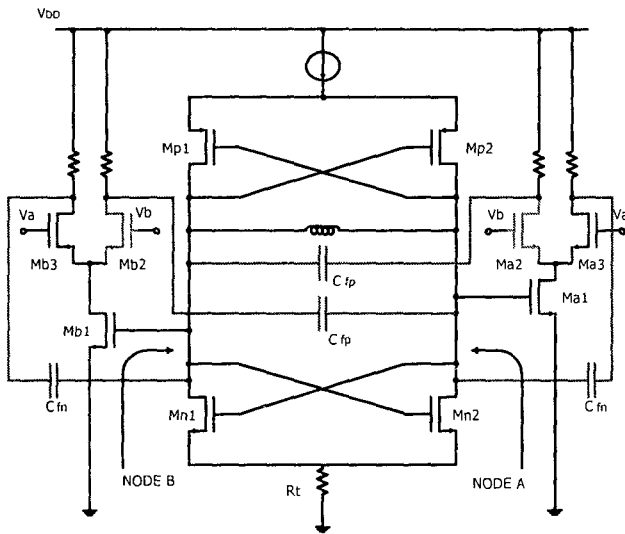


Fig. 8. Complete circuit of the proposed positive and negative feedback dual mode operation VCO.

Table 1. The summary of the simulation results of the proposed LC-oscillator.

Supply voltage	2.5 V
Tuning range	2.86 GHz ~ 2.45 GHz (Negative feedback) 2.86 GHz ~ 3.08 GHz (Positive feedback) (630 MHz)
Output power	-2.3 dBm (No feedback) -8.6 dBm (Negative feedback)
Technology	0.25um Standard CMOS technology

4. CONCLUSION

In this paper we proposed a new wide tuning range VCO topology using Miller capacitance. The differential LC oscillator structure results in 180 degree phase difference between two outputs which makes a positive feedback operation. The simulation shows that this proposed VCO has 410 MHz and 220 MHz frequency tuning range by negative and positive feedback mode. The tuning range is about 23% of the reference frequency.

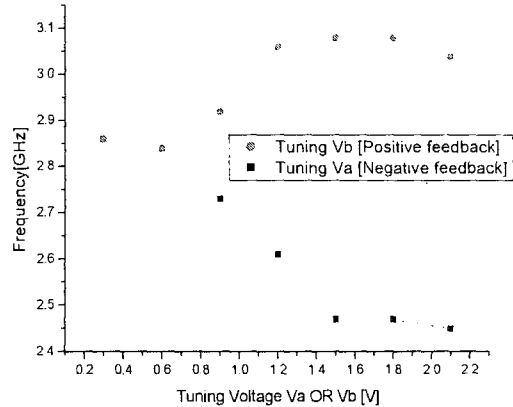


Fig. 9. Simulated tuning characteristics of the proposed VCO.

References

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