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Multirate Sampled-Data Control System: Optimal Digital Redesign Approach

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Abstract - This paper studies a multirate sampled-data control for LTI systems by using the digital redesign (DR) method. In this note, to well tackle the problem associated with both the state matching and the stabilization, our nobel strategy is to minimize the linear quadratic cost function. The main features of the proposed method are that i) the delta-operator-based descretization method is applied to improve the state-matching performance in the fast sampling limit and/or the large input multiplicity; ii) the proposed multirate control scheme can improve the state-matching performance in the long sampling limit; iii) some sufficient conditions that guarantee the stability of the closed-loop discrete-time system and provide a guarantee cost for the cost function can be formulated in the LMIs format; and iv) an optimal sampled-data controller in the sense of minimizing the upper bound of the cost function is also given by means of an LMI optimization procedure.

Key Words: Digital redisign(DR), sampled-data control, linear matrix inequalities (LMIs), multirate sampling.

1. Introduction

Digital redesign (DR) has gained tremendously increasing attention as yet another efficient design tool of sampled-data control [1]-[6]. The term DR involves converting a well-designed analog control into an equivalent digital one maintaining the property of the original analog control system in the sense of state-matching, by which the benefits of both the analog control and the advanced digital technology can be achieved.

This paper studies a multirate sampled-data control for LTI systems by using the DR method. In this note, we attempt to minimize the linear quadratic cost function for well tackling the problem associated with both the state matching and the stabilization, The main features of the proposed method four-fold. First. delta-operator-based descretization method is applied to improve the state-matching performance in the fast sampling limit and/or the large input multiplicity. Second, the proposed multirate control scheme can improve the state-matching performance in the long sampling limit. Third, some sufficient conditions that guarantee the stability of the closed-loop discrete-time system and provide a guarantee cost for the cost function can be formulated in the LMIs format. Finally an optimal sampled-data controller in the sense of minimizing the upper bound of the cost function is also given by means of an LMI optimization procedure.

2. Preliminaries

2. 1. Analog Control Systems

The plant is assumed to be LTI and have a state-space representation described by

$$\frac{d}{dt}x_{c}(t) = Ax_{c}(t) + Bu_{c}(t) \tag{1}$$

where x(t) is the state vector, and $u_c(t)$ is the digital control input.

The feedback controller is given by

$$u_{c}(t) = K_{c}x_{c}(t) \tag{2}$$

Then, the closed-loop system can take the form

$$\frac{d}{dt}x_c(t) = (A + BK_c)x_c(t) \tag{3}$$

Its solution at $t \in [kT, kT + T)$ is expressed by

$$x_{c}(kT+T) = \psi x_{c}(kT) \tag{4}$$

2. 2. Sampled-Data Control Systems

Multirate digital feedback control systems consisting of the plant and a state feedback digital controller are described by

$$\frac{d}{dt} x_d(t) = A x_d(t) + B u_d(t) \tag{5}$$

where x(t) is the state vector, and $u_d(t)$ is the digital control input. $u_d(t)$ is interconnected by A/D converter and D/A converter in which the operation speed of D/A converter is faster than one of A/D converter. If the periods of A/D and D/A are referred to T and T, respectively, the control actions alternate with a shorter period T and an input multiplicity N(=T/T). And

also, the digital control signals are fed into the plant with the ideal zeroth-order holds. Then, $u_d(t)$ is described by

$$u_d(t) = u_d(kT, lT') \tag{6}$$

 $t \in [kT + lT', kT + lT' + T'], l \in Z_{[0, N-1]} = \{0, 1, \dots, N-1\},$ for where

$$u_d(kT, lT') = K \alpha(kT, 0)$$

3. Main Results

3.1 Fast Discretization of Sampled-data System Using Delta-operator

To develop the discretized version of (1), we apply the the fast discretization technique [7] to the sampled-data system (1). The fast discretization leads to a multirate discrete-time system which can be lifted to a single-rate discrete-time system. In specific, a multirate discrete-time plant model of (1) is first derived, and then a lifted system is constructed.

Connecting the fast-sampling operator and the fast-hold operator with $[kT+lT', kT+lT'+T'], (k, l) \in \mathbb{Z}_{\geq 0} \times \mathbb{Z}_{[0,N-1]}$, to (1) leads the multirate discrete-time plant model. The next results presents the multirate discretized version of (1).

Proposition 1: The multirate discrete-time model of the sampled-data system (1) can be given by

$$\delta x_{d}(kT, lT') = G_{\delta}x_{d}(kT, lT') + H_{\delta}u_{d}(kT, lT')$$
for $[kT + lT', kT + lT' + T'), (k, l) \in Z_{\geq 0} \times Z_{\{0, N-1\}}$, where

$$G_{\delta} = \frac{G - I}{T}$$
 and $H_{\delta} = (G - I)A_{i}^{-1}B_{i}T$.

To transform the multirate discrete-time system (8) into the single-rate one, we invoke the discrete-time lifting. The next proposition states a discrete-time system discretized by the multirate sampling control (8).

Proposition 2: Given a multirate discrete-time system () for $l \in \mathbb{Z}_{[0,N-1]}$, a lifted sampled inpu

$$\overline{u}_{d}(kT,0) = \begin{bmatrix} u_{d}(kT,0) \\ u_{d}(kT,T') \\ \vdots \\ u_{d}(kT,NT'-T') \end{bmatrix}$$
(9)

leads a lifted system

$$\delta x_{d}(kT,0) = \mathcal{T}_{\delta} x_{d}(kT,0) + \mathcal{H}_{\delta} \tilde{u}_{d}(kT,0) \qquad (10)$$

for $t \in [kT, kT + T)$, where

$$G_{\delta} = \frac{G^{N} - I}{T},$$

$$\mathcal{H}_{\delta} = \frac{1}{T} [G^{N-1} H G^{N-2} H \cdots H]$$

Corollary 1: In the analog control system (3),

 the multirate discrete-time model can take the form $\delta x_c(kT,lT') = \phi_{\delta} x_c(kT,lT')$ (11)

for $t \in [kT + lT', kT + lT' + T']$, where $\phi_b = \frac{\phi - I}{T'}$.

• the lifted system can take the form

$$\delta x_c(kT,0) = \mathcal{F}_{\delta} x_c(kT,0) \tag{12}$$

for $t \in [kT, kT + T)$, where $\widetilde{\Phi}_k = \frac{\Phi^{N} - I}{T}$

3.2 Optimal Digital Redeign

Our goal is to find K_I so that the closed-loop state $x_{d}(t)$ matches the closed-loop state $x_{c}(t)$ at every sampling instant T as closely as possible, guaranteed stability. To consider the closed-loop $x_c(t)$ at every sampling instant T, transferring (12) from T to T' leads

$$\delta \widetilde{x}_{c}(kT,0) = \overline{\phi}_{k} x_{c}(kT,0) \tag{13}$$

where

$$\delta \widetilde{x}_{c}(kT,0) = \left[\frac{x_{c}(kT,T')^{T} - x_{c}(kT,0)^{T}}{T}, \cdots, \frac{x_{c}(kT,NT')^{T} - x_{c}(kT,0)^{T}}{NT'} \right]^{T}$$

and

$$\overline{\phi}_{\delta} = \begin{bmatrix} \overline{\phi}_{\delta 0} \\ \overline{\phi}_{\delta 1} \\ \vdots \\ \overline{\phi}_{\delta N-1} \end{bmatrix} = \begin{bmatrix} \frac{\phi - I}{T} \\ \frac{\phi^2 - I}{2T} \\ \vdots \\ \frac{\phi^N - I}{NT} \end{bmatrix}$$

In the same manner, we can capture the state T by transferring from (10) to the following model:

$$\delta \tilde{x}_d(kT,0) = \overline{G}_{\delta} x_d(kT,0) + \overline{H}_{\delta} \tilde{u}_d(kT,0)$$
 (14)

where

$$\delta \tilde{x}_{d}(kT,0) = \left[\frac{x_{d}(kT,T')^{T} - x_{d}(kT,0)^{T}}{T}, \cdots, \frac{x_{d}(kT,NT')^{T} - x_{d}(kT,0)^{T}}{NT} \right]^{T}$$

$$\overline{G}_{\delta} = \begin{bmatrix} \overline{G}_{\delta 0} \\ \overline{G}_{\delta 1} \\ \vdots \\ \overline{G}_{\delta N-1} \end{bmatrix} = \begin{bmatrix} \frac{G-I}{T} \\ \frac{G^2-I}{2T} \\ \vdots \\ \frac{G^N-I}{NT} \end{bmatrix}$$

and

$$\begin{split} \overline{H}_{\delta} &= \begin{bmatrix} \overline{H}_{\delta 0} \\ \overline{H}_{\delta 1} \\ \vdots \\ \overline{H}_{\delta N-1} \end{bmatrix} \\ &= \begin{bmatrix} \underline{H} & 0 & \cdots & \cdots & 0 \\ \underline{GH} & \underline{H} & 0 & \cdots & 0 \\ \underline{GSH} & \underline{H} & 0 & \cdots & 0 \\ \vdots & \vdots & \cdots & \cdots & 0 \\ \underline{G}^{N-1}\underline{H} & \underline{G}^{N-2}\underline{H} & \cdots & \cdots & \underline{H} \\ NT & NT & NT \end{bmatrix} \end{split}$$

In sequel, our main problem for the system (14) is the problem of designing a multirate feedback control law

$$\widetilde{u}_{d}(kT,0) = \widetilde{K}_{d}x(kT,0) \tag{15}$$

 $K_d = \left[K_0^T K_1^T \cdots K_{N-1}^T\right]^T$, such that i) the origin x=0 is a globally asymptotically stable equilibrium point of the closed-loop system

 $\delta \tilde{x}_d(kT,0) = (\overline{G}_{\delta} + \overline{H}_{\delta} K_d) x_d(kT,0)$ (16) and ii) by comparing (13) and (16), to realize $\delta \tilde{e}(kT,0) = \delta \tilde{x}_c(kT,0) - \delta \tilde{x}_d(kT,0) = 0$ under the assumption $x_c(kT,0) = x_d(kT,0)$ is numerically synthesized for $\|\delta \tilde{e}(kT,0)\|$ to be a minimizer in the induced 2-norm sense.

To well tackle the problem associated with both the state matching and the stabilization problems, our strategy is to minimize the following cost function

$$J = \sum_{k=0}^{\infty} \left(x_d^T(kT, 0) Q x_d(kT, 0) + \delta \tilde{e}^T(kT, 0) R \delta \tilde{e}(kT, 0) \right)$$

where $Q \ge 0$ and R > 0 are given weighting matrices.

Remark 1: Minimizing J corresponds in some sense to keeping $x \not kT.0$) and $\delta \vec{e}(kT.0)$ close to zero. If it is more important to us that the state $x \not kT.0$) be small, then we should choose Q large to weight it heavily in J, which we are trying to minimize. If it is more important that the error state $\delta \vec{e}(kT.0)$ be small for the state matching, then we should select R to be $R \not Q$. From (13) and (16), J in (17) for every $I \in Z_{\{0,N-1\}}$ can take the form

$$J = \sum_{k=0}^{\infty} x_{d}^{T}(kT,0) \left(Q + \left(\overline{\phi}_{\delta l} - \overline{G}_{\delta l} - \overline{H}_{\delta l} K_{d} \right)^{T} \times R \left(\overline{\phi}_{\delta l} - \overline{G}_{\delta l} - \overline{H}_{\delta l} K_{d} \right) \right) x_{d}(kT,0)$$

To achieve an optimal digital redesign, we consider the multirate sampled-data control problem of minimizing an upper bound of J in (18) for the system (13) and (16).

Theorem 1: For the system (13) and (16), if there exist Z, V, $X = X^T > 0$, and M_d with appropriate dimension, such that the linear matrix inequalities (19), where $(\cdot)^T$ denotes the transposed element in symmetric position, hold then, $K_d = M_d Z^{-1}$ is a stabilizing periodic feedback gain with which J in (18) of the closed-loop system (16) satisfies

$$J \le x_0^T \frac{X}{T} x_0$$

Furthermore, if x_0 is a random variable satisfying

$$E\{x_0\} = 0, \quad E\{x_0x_0^T\} = I$$

where $E(\cdot)$ denotes the expectation operator. an optimal feedback gain can be obtained by solving the following optimization

minimize z, x, \mathcal{M}_{d}, V trace(V)

subject to linear matrix inequalities () and

$$\begin{bmatrix} -V & (\cdot) & T \\ I & -X \end{bmatrix} < 0$$

4. Concluding Remark

This paper studies a multirate sampled-data control for LTI systems by using the digital redesign (DR) method. This paper proposed that nobel strategy to well tackle the problem associated with both the state matching and the stabilization is to minimize the linear quadratic cost function.

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$$\begin{bmatrix} \frac{X}{T} - Z - Z^T & (\cdot)^T (\cdot)^T (\cdot)^T \\ R^{\frac{1}{2}} \overline{\phi}_{\delta l} Z - R^{\frac{1}{2}} \overline{G}_{\delta l} Z - R^{\frac{1}{2}} \overline{H}_{\delta l} \mathcal{M}_d & -I (\cdot)^T (\cdot)^T \\ Q^{\frac{1}{2}} Z & 0 & -I (\cdot)^T \\ \frac{Z}{T} + \overline{G}_{\delta l} Z + \overline{H}_{\delta l} \mathcal{M}_d & 0 & 0 - \frac{X}{T} \end{bmatrix} \langle 0 \qquad l \in N_{[0, N-1]}$$
(19)