

In-Situ Heat Cooling using Thick Graphene and Temperature Monitoring with Single Mask Process

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Abstract

In this paper, in-situ heat cooling with temperature monitoring is reported to solve thermal issues in electric vehicle (EV) batteries. The device consists of a thick graphene cooler on top of the substrate and a platinum-based resistive temperature sensor with an embedded heater above the graphene. The graphene layer is synthesized by using chemical vapor deposition directly on the Ni layer above the Si substrate. The proposed thick graphene heat cooler does not use transfer technology, which involves many process steps and does not provide a high yield. This method also reduces the mechanical damage of the graphene and uses only one photomask. Using this structure, temperature detection and cooling are conducted simultaneously using one device. The temperature coefficient of resistance (TCR) of a $1 \times 1 \text{ mm}^2$ temperature sensor on 1- μm -thick graphene is $1.573 \times 10^3 \text{ ppm}/^\circ\text{C}$. The heat source cools down 7.3°C from 54.4°C to 47.1°C .

Keywords: Thick Graphene, Heat Cooler, Temperature Sensor, TCR, Single Mask Process

1. INTRODUCTION

Thermal issues in electric vehicle (EV) batteries or 3D integrated circuits (ICs) have become more important. For batteries for EV applications, the energy storage capacity is reduced by 35%, when the operating temperature of the battery cell increased to 55°C . The storage capacity is also reduced operating temperatures of less than -20°C . An exothermic reaction in the battery can form hotspots, which could result in self-heating or asymmetrical current flow. In addition, the hotspots are the prime cause of thermal runaway, which could cause an explosion of the battery. To ensure the lifetime, performance, and safety of the battery, the operating temperature range of $35^\circ\text{C} - 40^\circ\text{C}$ should be maintained using thermal management [1-3]. For battery thermal management in EVs, research on temperature sensors to monitor the temperature of the battery cell surface and on the cooling layer of the graphite sheet on the battery cell surface to

cool down the temperature are in progress. However, in these studies, temperature monitoring and heat cooling require two separate devices [4-6]. For 3D ICs, as the integration density increases, the heat density also increases. The small footprint results in a small amount of heat spreading over a small heat sink area, which cannot effectively cool down the chip. To cool down the generated heat in the chips, heat spreading or heat sink structures are necessary [7].

To overcome these thermal issues, many studies using graphene, which exhibits high thermal conductivity have been reported [8-11]. At Chalmers University of Technology, the temperature of the heat source decreased from 121°C to 108°C using a mono layer of graphene synthesized on a Cu thin film using chemical vapor deposition (CVD). The graphene was transferred using a polymethyl methacrylate (PMMA) supported wet chemical process. At Seoul National University, the heat source temperature was reduced from 57.49°C to 48.43°C using thick graphene synthesized on Ni foil transferred using thermal release tape (TRT) and hot pressing. These studies were conducted using the conventional transfer method, which involves five process steps. This conventional transfer method has some disadvantages. The graphene layer is difficult to align on the target substrate because the transfer is conducted manually. In addition, after transferring, the graphene layer is not attached perfectly on the substrate. These disadvantages result in a low yield and low thermal management performance.

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In this paper, with the in-situ heat-cooling layer of thick graphene in a temperature-monitoring sensor, multiple-functions, i.e., monitoring the temperature in real time and cooling down of the generated heat, can be performed simultaneously using only one device. To fabricate a thick graphene heat cooler, a thick layer of graphene was synthesized directly using CVD on the Ni layer above a Si wafer. After the synthesis, a dielectric layer was deposited, and the temperature sensor was fabricated. The heat-cooling layer using graphene on the substrate process step was reduced to two steps, Ni layer deposition, and graphene synthesis. Because the Ni layer was not eliminated, the graphene layer adhered to the substrate completely. This method can overcome the low yield of the conventional transfer method.

2. DESIGN AND FABRICATION

Fig. 1 shows the device schematic. The Ni layer above the substrate plays an important role as a seed layer to synthesize the thick graphene layer. The SiO₂ layer is deposited for insulation and planarization on the graphene layer. The temperature sensor on the SiO₂ layer is the resistance temperature detector (RTD) type. The sensor surrounds the embedded heater. The sensor material is platinum, which exhibits a high melting point, stability, and linearity. Based on the resistance changes with temperature in Eq. (1), the sensor detects the temperature:

$$TCR = \frac{dR}{dT} \times \frac{1}{R_0} \quad (1)$$

The device was fabricated on a 4-inch Si wafer. The heat-cooling layer using 1- μ m-thick graphene was synthesized by CVD on the Ni layer above the Si substrate. The platinum-based temperature sensor was fabricated using a one-mask simple

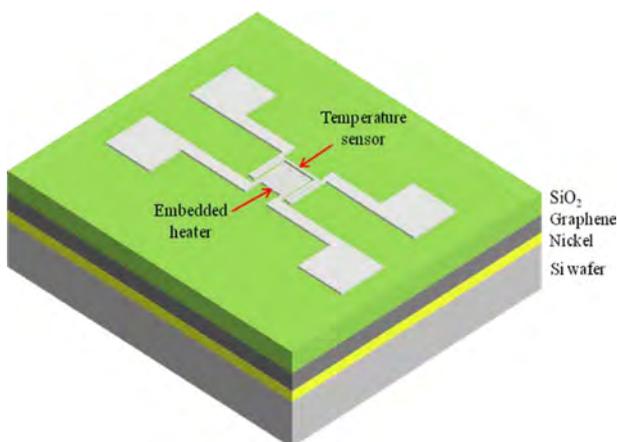


Fig. 1. Device schematic.

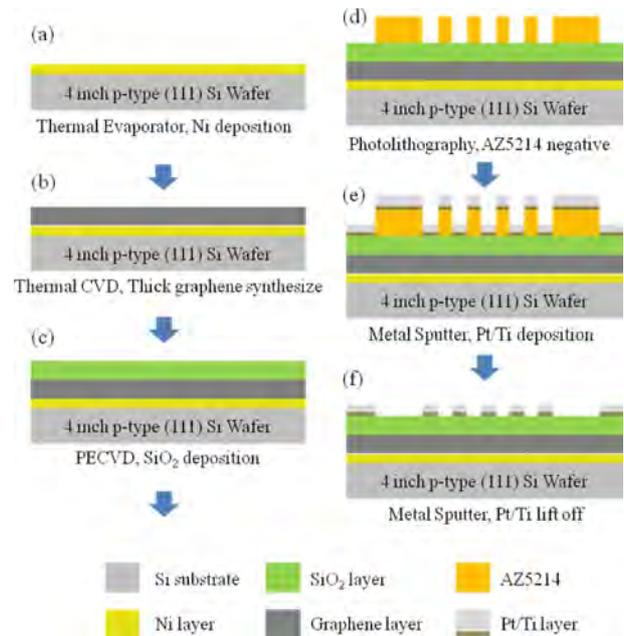


Fig. 2. Fabrication process of in-situ heat cooling layer in temperature monitoring sensor system

- (a) 500-nm-thick Ni layer deposition using thermal evaporator for graphene synthesis
- (b) Thick graphene synthesis using thermal CVD
- (c) SiO₂ deposition for insulation and planarization
- (d) Photolithography for temperature sensor pattern
- (e) 100 nm / 20-nm-thick Pt / Ti deposition
- (f) Lift-off procedure for Pt/Ti temperature sensor.

process on the graphene cooling layer.

Fig. 2 shows the fabrication process. For fabricating a thick graphene layer, a 500-nm-thick Ni layer was deposited using a thermal evaporator. Then, 1- μ m-thick graphene was synthesized using thermal CVD followed by the deposition of a 1- μ m-thick SiO₂ layer for insulation and planarization. To make the sensor pattern, a Pt/Ti layer was deposited by sputtering, and the temperature sensor was prepared using the lift-off process. Two samples were prepared to measure the temperature cooling: one with 1- μ m-thick graphene and the other with no graphene.

3. RESULTS AND DISCUSSION

The resistance of the temperature sensor was measured to calculate the TCR using Eq. (1) according to the change in the temperature. The measurements were performed using the same power applied to the embedded heater both with and without the graphene cooling layer followed by calculating the sensing temperature.

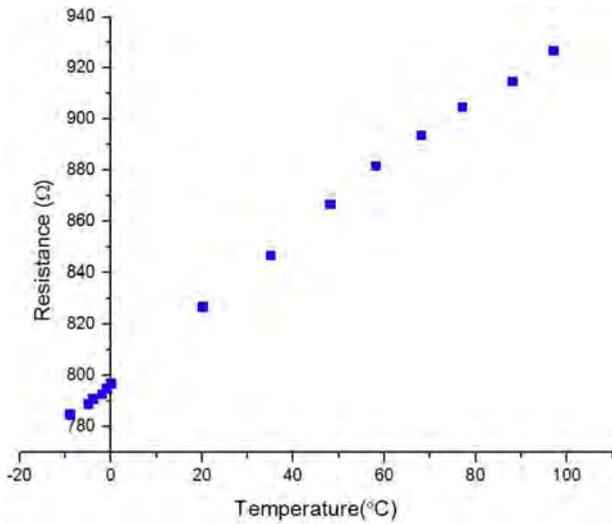


Fig. 3. Resistance vs. temperature characteristic of the sensor

3.1 Sensor characteristic

The RTD type sensor was characterized by TCR. Fig. 3 displays the resistance measurements for the same sensor with the temperature ranging from -9°C to 90°C, where the temperature was measured 5 times. The device uses graphene as a heat-cooling layer and shows good linearity as well as repeatability. The average value of the resistance at 20°C was 827 Ω. The maximum difference for five measurements was 3 Ω, which was less than 1%. The average value of dR/dT, which was calculated from the slope of the linear graph, was 1.3Ω/°C. Each dR/dT value has an error range of less than 4.6% from the average value.

As the temperature increased, the resistance of the temperature sensor also increased linearly, and the average correlation coefficient was 0.99. The average TCR, which was calculated using Eq. (1), was 1.573×10^3 ppm/°C.

3.2 Temperature cooling

The temperature cooling could be measured using the two samples mentioned in section 2 above. The same power was applied to the embedded heater of each structure, and the sensor resistances, R_o and ΔR , were measured for both samples, which can be converted to a temperature change of the heater for both cases with and without the graphene cooling layer, as shown in Eq. (2). In this calculation, the TCR from Eq. (1) is used.

$$\Delta T_{w/heatcooler} = \frac{\Delta R_{w/heatcooler}}{TCR_{w/heatcooler} \times R_{o,w/heatcooler}} \quad (1)$$

Table 1. Temperature according to the input power

Input power	Without heat cooler	With heat cooler
0.45W	37.7°C	34.6°C
1.276W	54.4°C	47.1°C

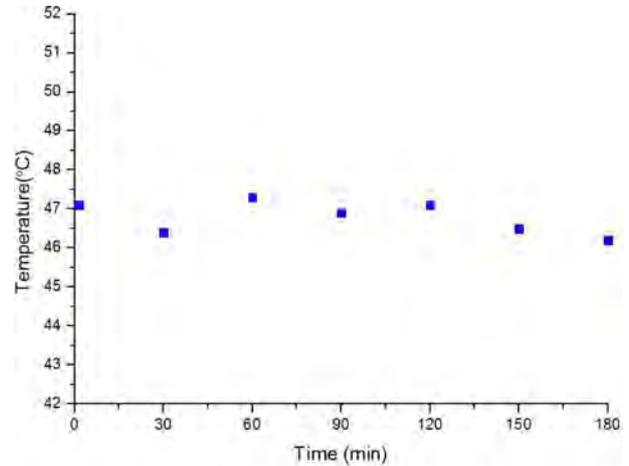


Fig. 4. Temperature of the sensor with heat cooler structure vs. time.

$$\Delta T_{w/o_heatcooler} = \frac{\Delta R_{w/o_heatcooler}}{TCR_{w/o_heatcooler} \times R_{o,w/o_heatcooler}} \quad (2)$$

The TCRs of both samples were 1.573×10^3 ppm/°C and 1.764×10^3 ppm/°C with and without graphene, respectively. A power of 1.276 W was applied to the embedded heater of the sample without graphene to increase the temperature to 54.4°C. The temperature of the device with the graphene heat cooler was 47.1°C. The temperature cooling was 7.3°C, which is the temperature difference between the samples. The same measurement was performed for a lower power of 0.45 W. Table 1 shows the temperature cooling based on the heat cooling effect of graphene due to its very high thermal conductivity. Therefore, we can expect larger cooling for a higher operating temperature.

The cooling performance of the device over time was also characterized by maintaining the input power of the device at 1.276 W for 3 h. The temperature fluctuation was less than 1.3%, as observed in Fig. 4.

4. CONCLUSIONS

In this paper, in-situ heat cooling using a thick graphene layer with simultaneous temperature monitoring was proposed to solve thermal issues in EV batteries or ICs. This simple device exhibits two functions simultaneously: real-time temperature detection and cooling down of the heat source. While measuring the temperature

for 3 h, the heat cooler can also cool the heat source.

The heat cooler of the thick graphene layer was synthesized using CVD directly on the Ni layer above the Si substrate. The heat cooler does not use the conventional transfer method. Therefore, it could reduce mechanical damage of the graphene as well as the number of processing steps.

The platinum-based temperature sensor was fabricated by a single mask simple process on a thick graphene cooler. It exhibited good linearity and repeatability. With the power of 1.276 W, the heater temperature cooled down by 7.3°C with very little fluctuation.

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